

Interaction between a synthetic jet and turbulent boundary layers

B. Ganapathisubramani*

*Aerodynamics and Flight Mechanics Group, University of Southampton



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T. A. Berk*, G. Jankee*
B. Ganapathisubramani*

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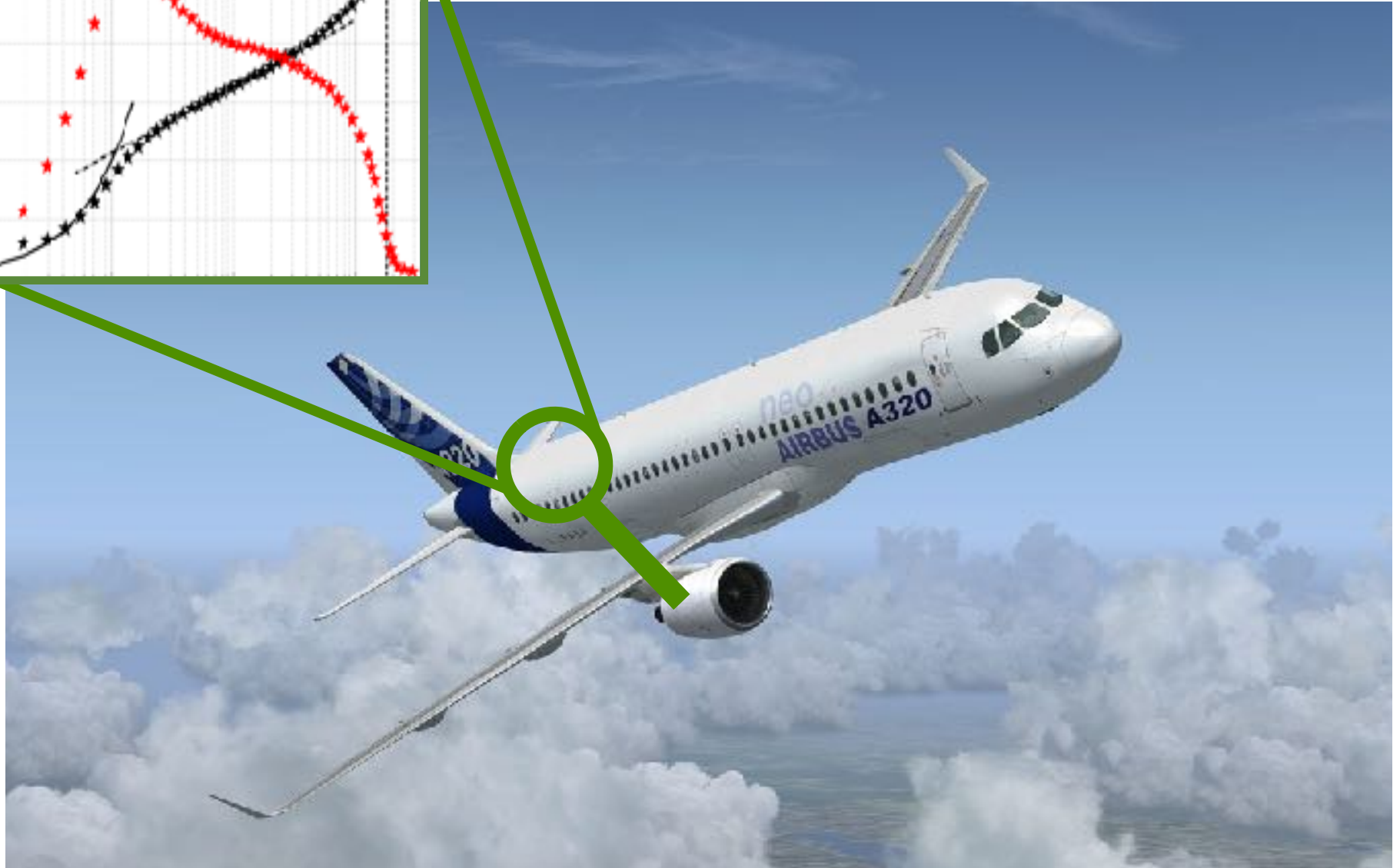
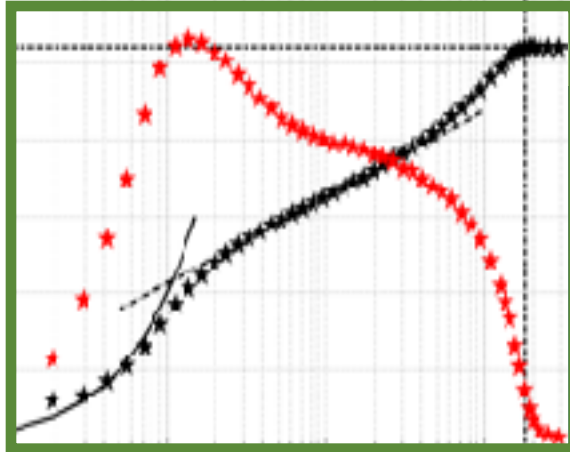
Interaction between a synthetic jet and turbulent boundary layers

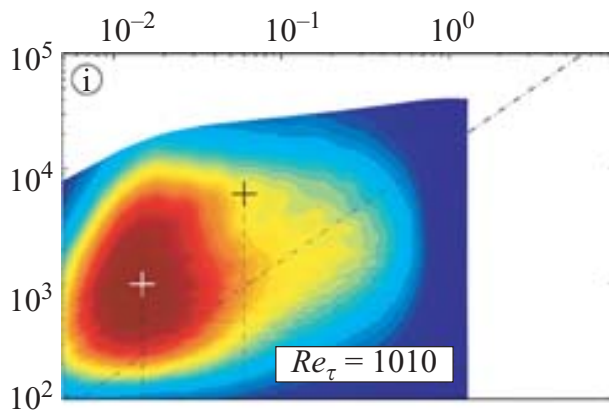
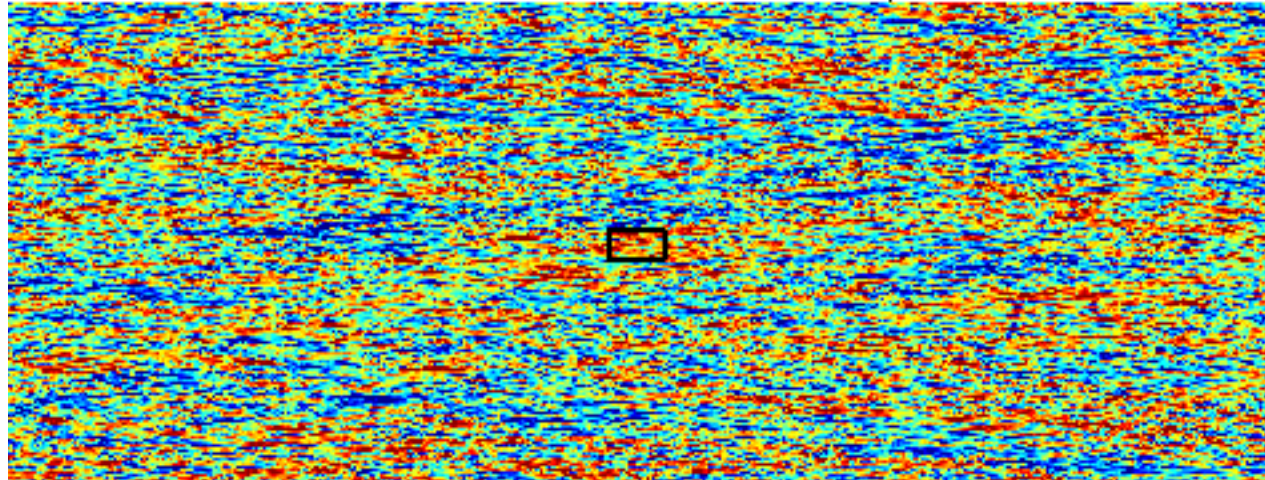
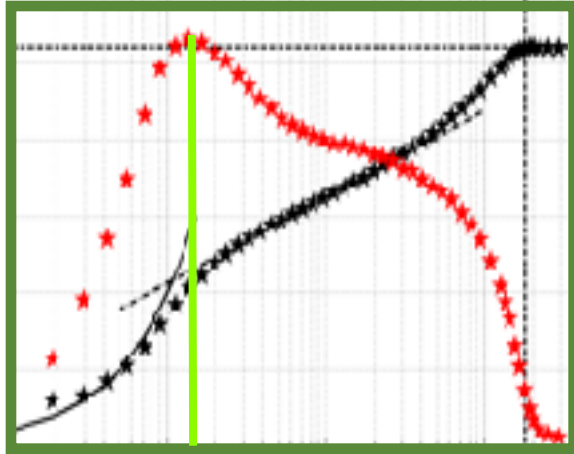
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B. Ganapathisubramani*

N. Hutchins¹, I. Marusic¹

*Aerodynamics and Flight Mechanics Group, University of Southampton

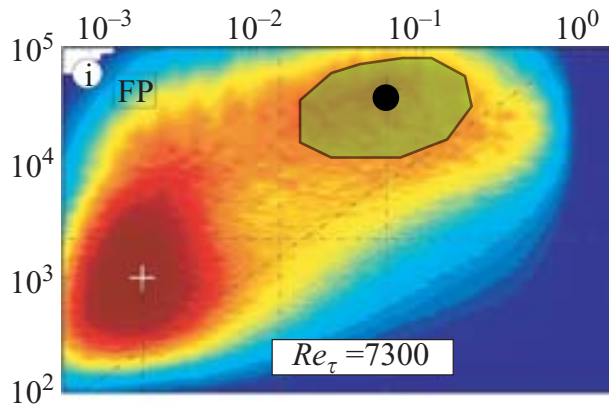
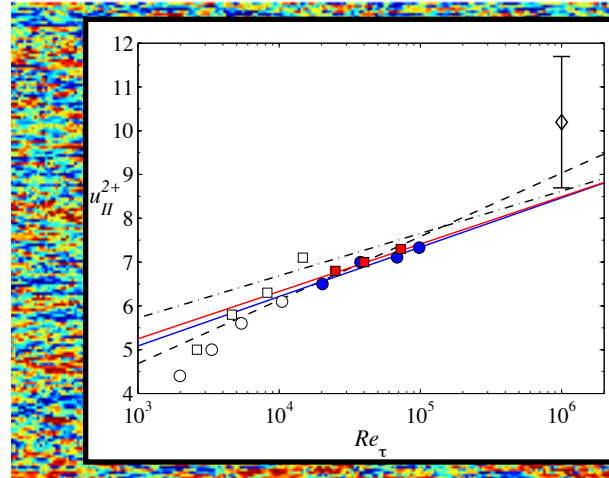
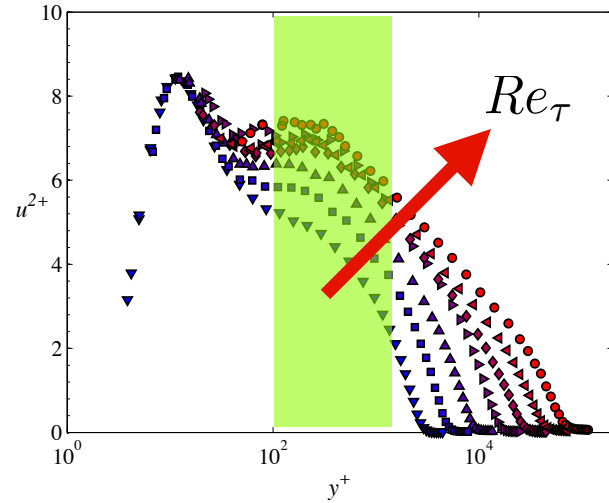
¹Department of Mechanical Engineering, University of Melbourne



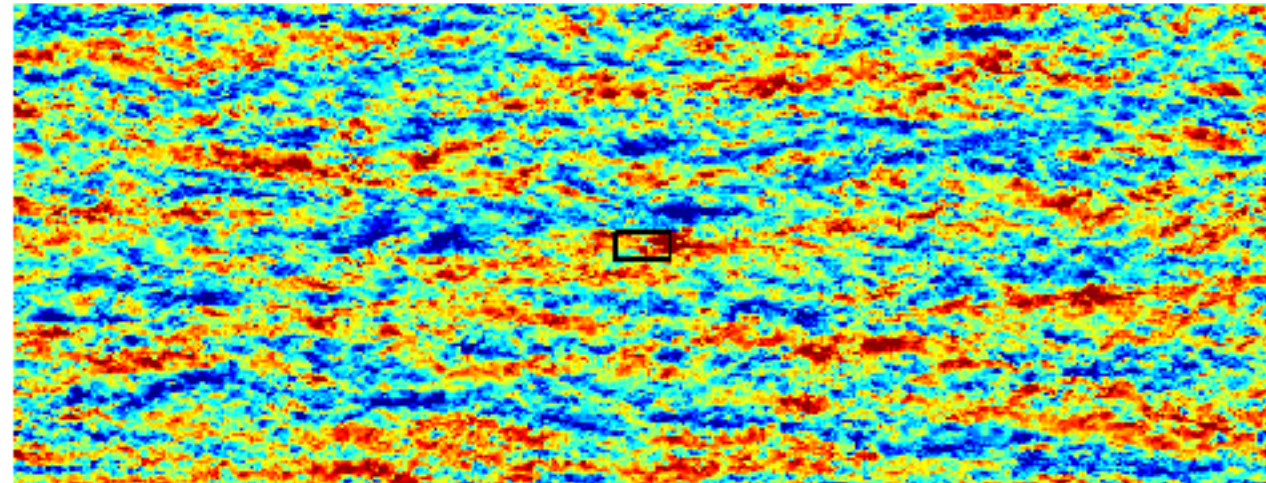


Near-wall control is the only demonstrated strategy

Valikivi, Hultmark & Smits (2015)



Hutchins & Marusic (2007)

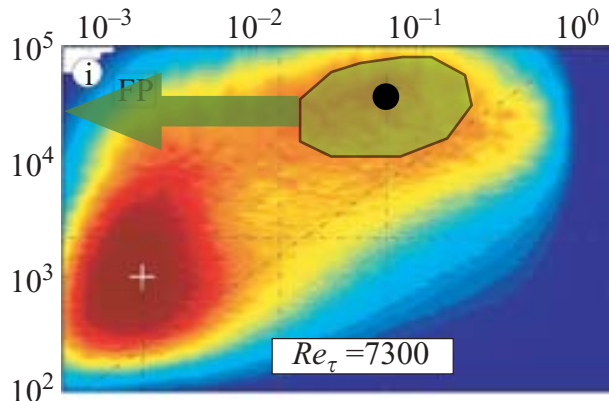
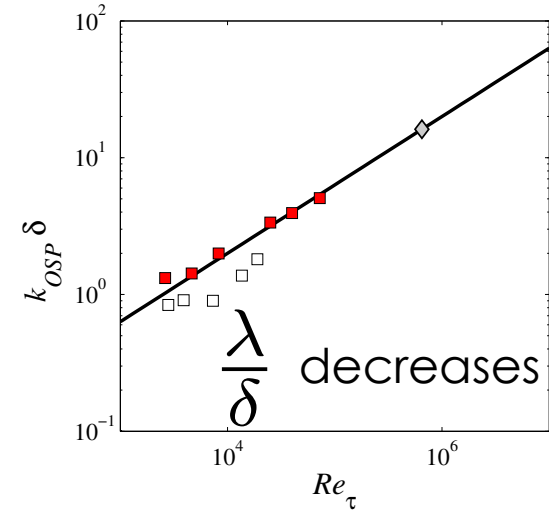
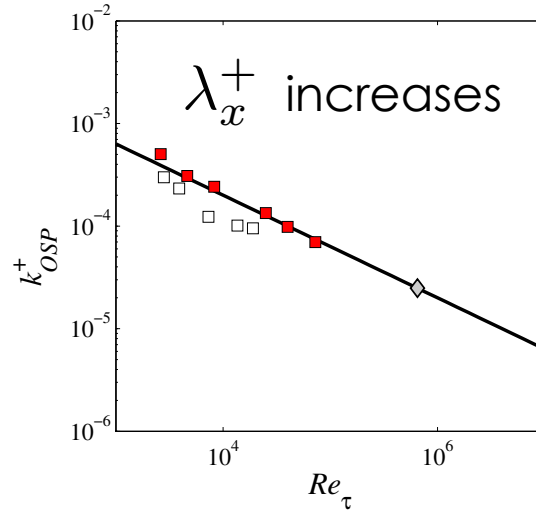
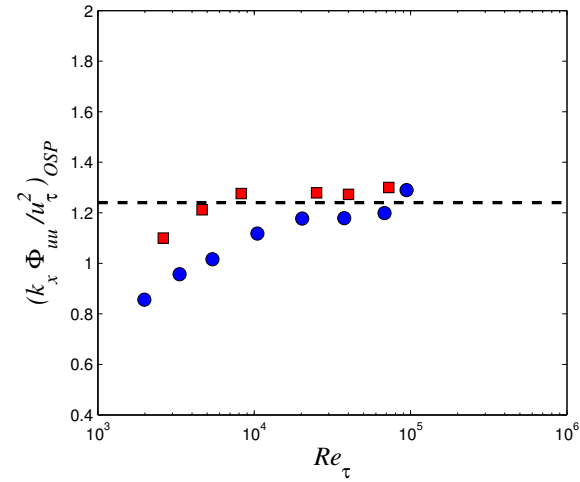


$$Re_\tau = \frac{\delta U_\tau}{\nu}$$

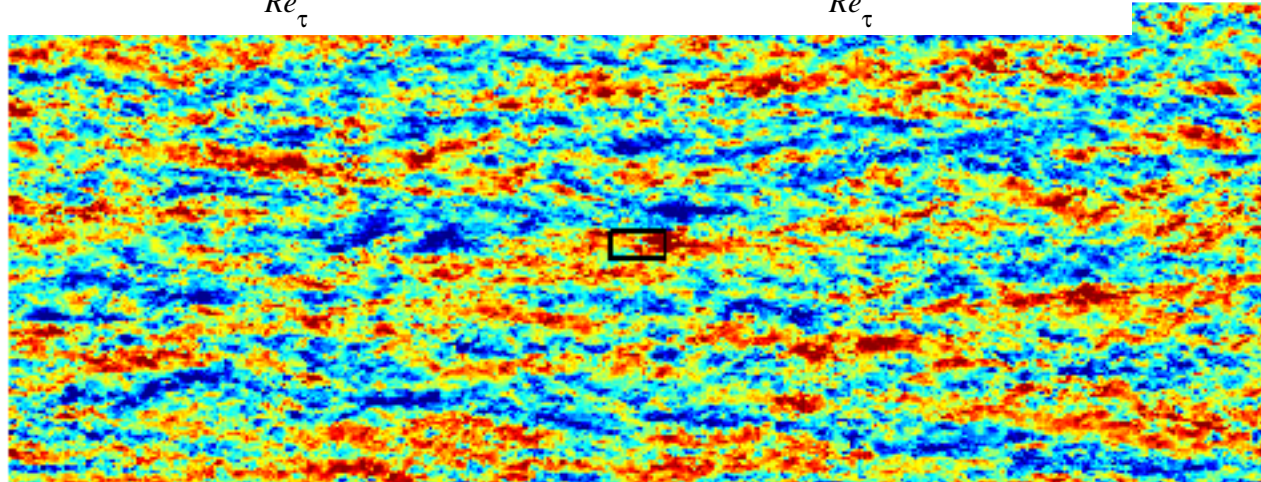
$$Re_\tau \approx 1000, \quad \frac{\lambda_{LS}}{\lambda_{SS}} \approx 1 \quad \lambda_{SS}^+ \approx 1000 \quad \lambda_{LS} \approx \delta$$

$$Re_\tau \approx 5000, \quad \frac{\lambda_{LS}}{\lambda_{SS}} \approx 5$$

Valikivi, Ganapathisubramani & Smits (2015)



Hutchins & Marusic (2007)



Can we control this footprint to reduce drag?

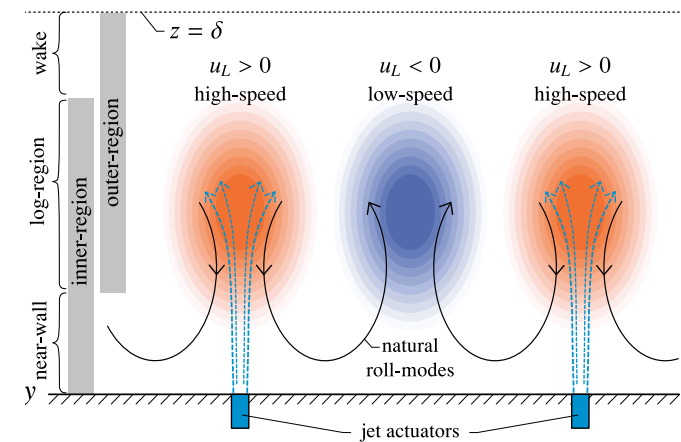
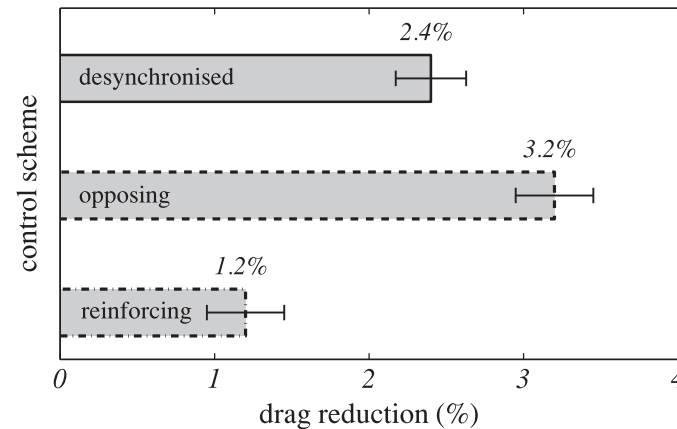
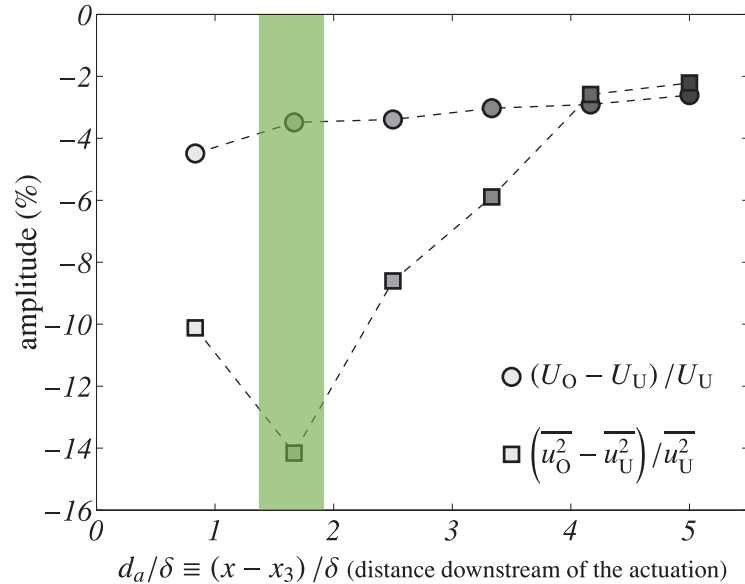
If so, what are the actuator requirements?



Skin-friction drag reduction in a high-Reynolds-number turbulent boundary layer via real-time control of large-scale structures

M.R. Abbassi, W.J. Baars*, N. Hutchins, I. Marusic

Department of Mechanical Engineering, The University of Melbourne, Melbourne 3010, Victoria, Australia



Effectiveness:

- jet trajectory
- jet decay

Can we control this footprint to reduce drag?

If so, what are the actuator requirements?

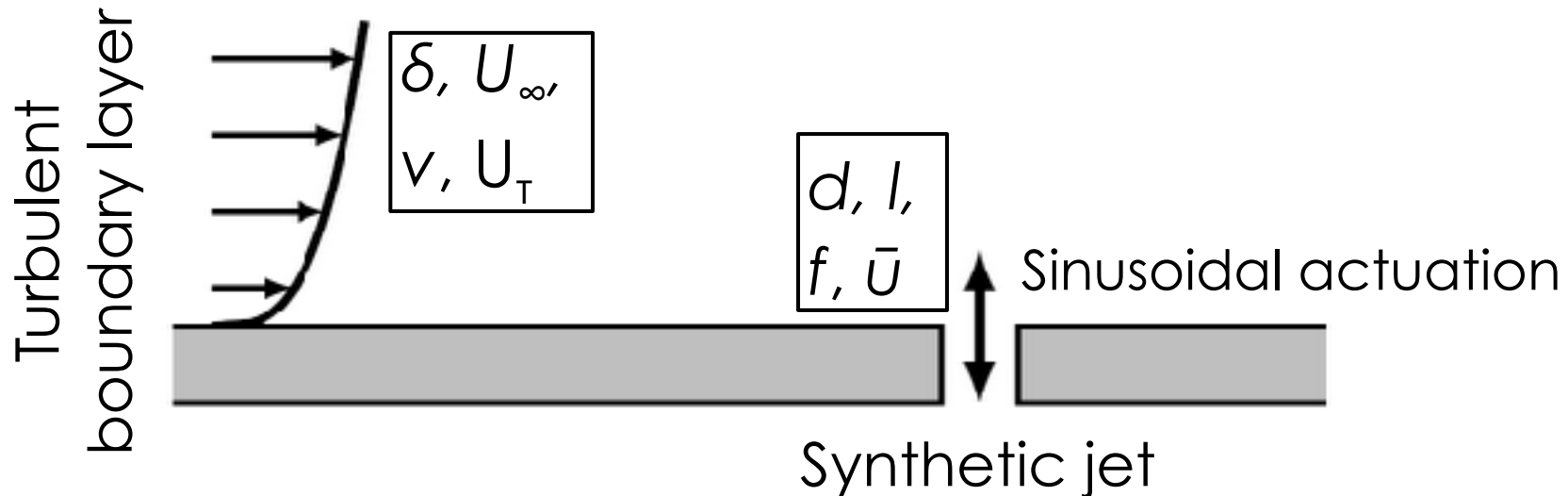
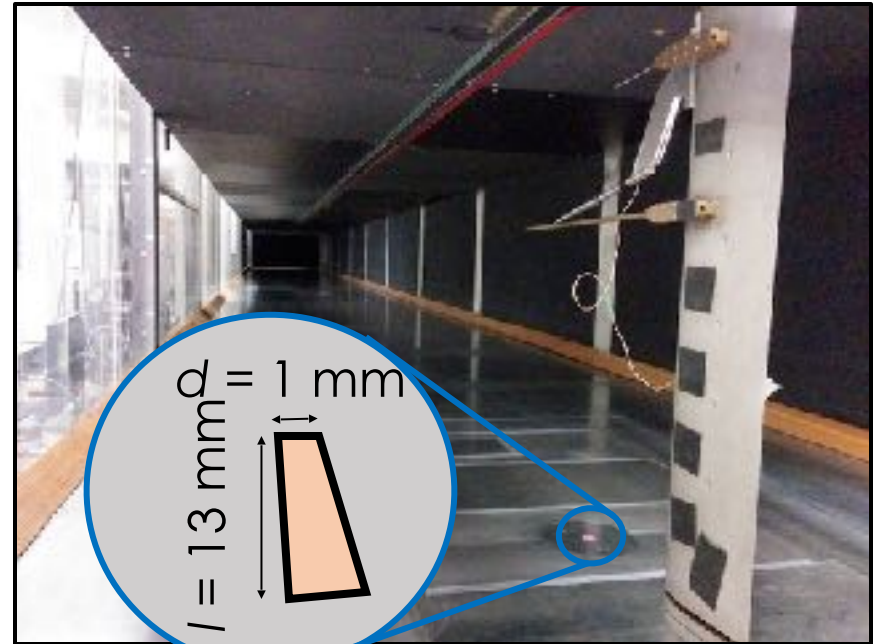
How does a synthetic/pulsed jet evolve in a turbulent boundary layer?

Jet trajectory: Facility

High-Reynolds number
boundary layer wind tunnel



0.9 m x 1.9 m x 27 m
 Re_τ : 1000 - 25000

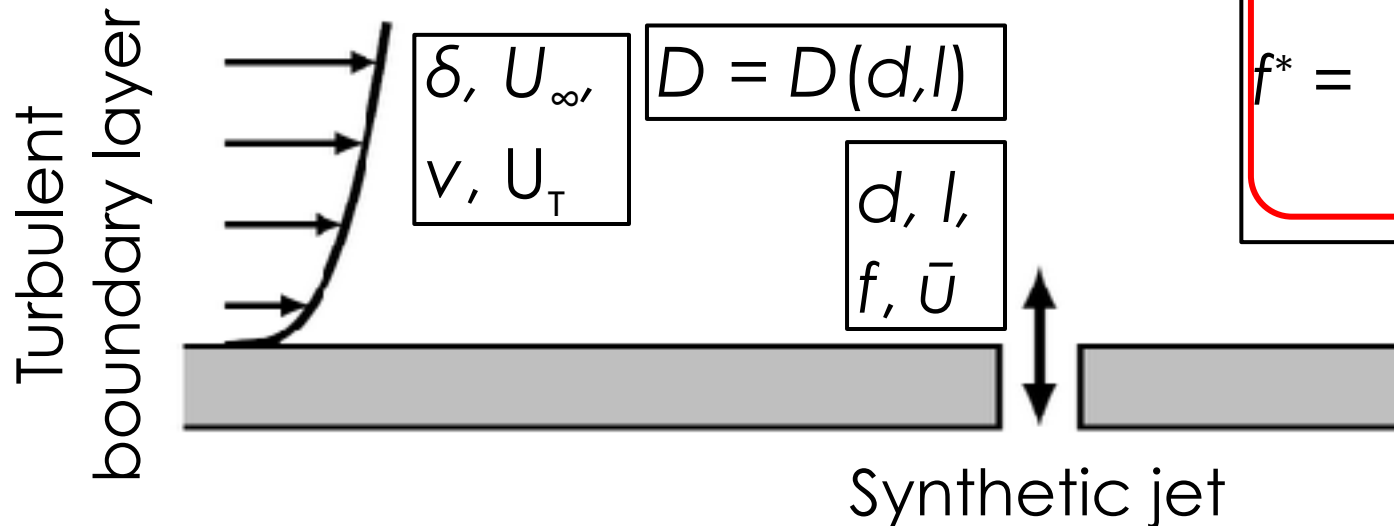


Jet trajectory

Important parameters

Proper scaling of f ?

Variation of trajectory with f^* , r and Re_T ?



TBL:

$$Re_T = U_T \delta / \nu$$

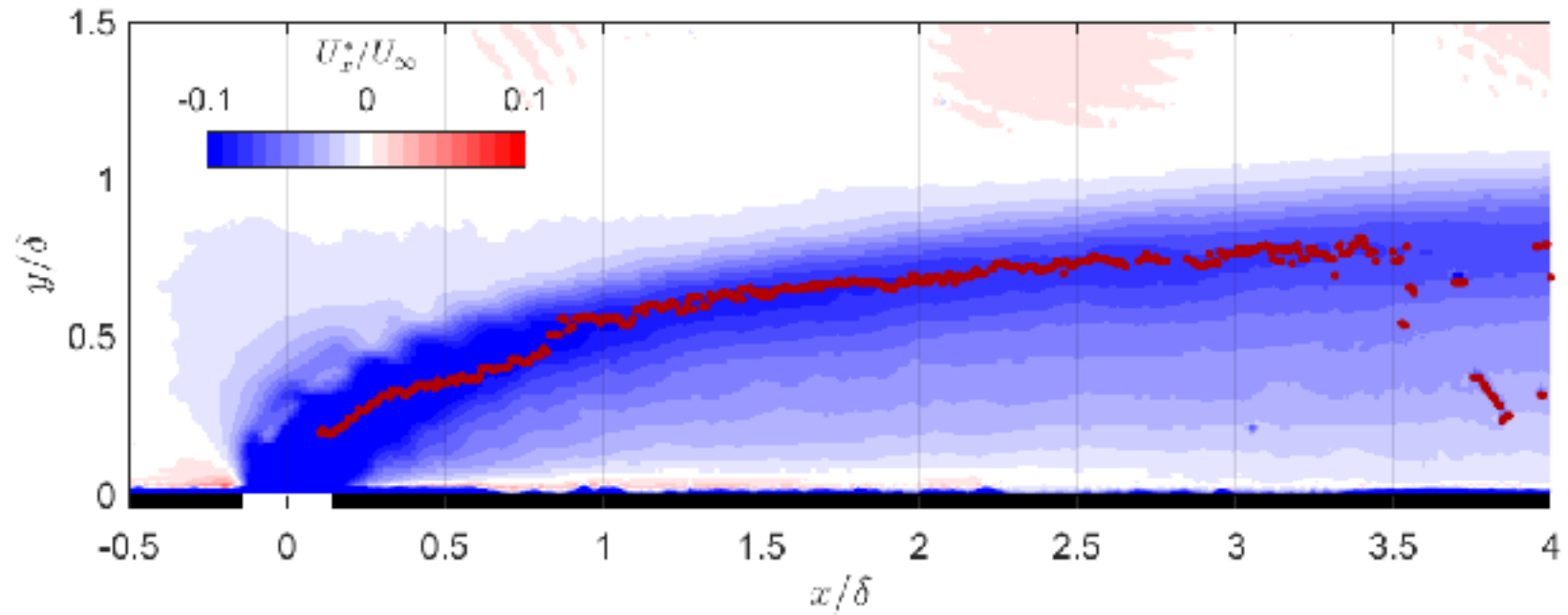
Synthetic jet:

$$AR = l/d = 13$$

Interaction:

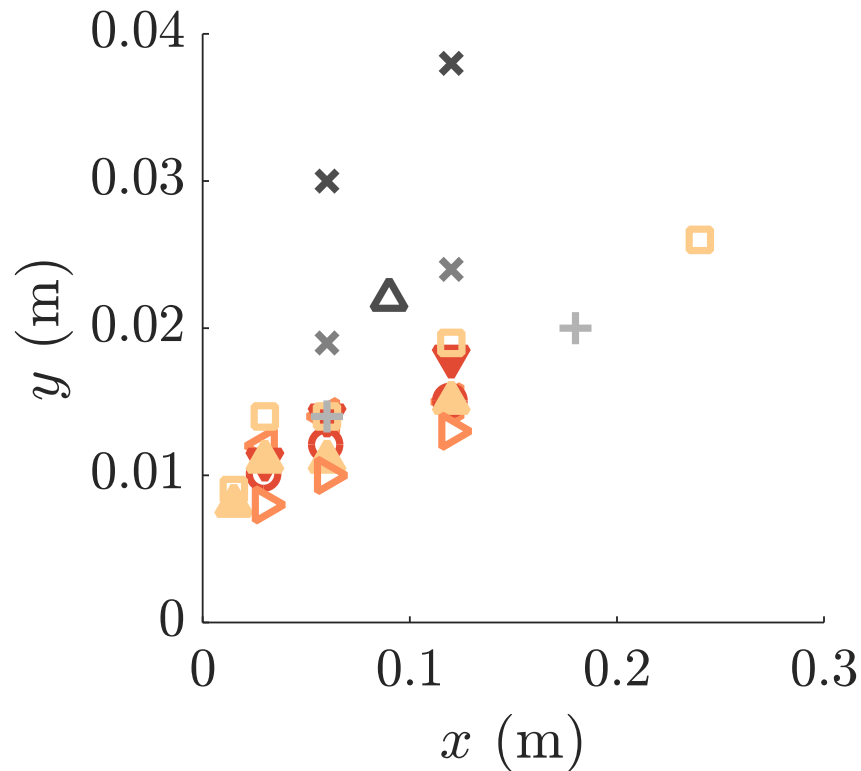
$$r = \bar{u} / U_\infty$$

$$f^* = \begin{cases} f \delta / U_\infty \\ f \nu / U_T^2 \\ f D / U_\infty \end{cases}$$



Trajectory measured from hot-wire measurements matches PIV

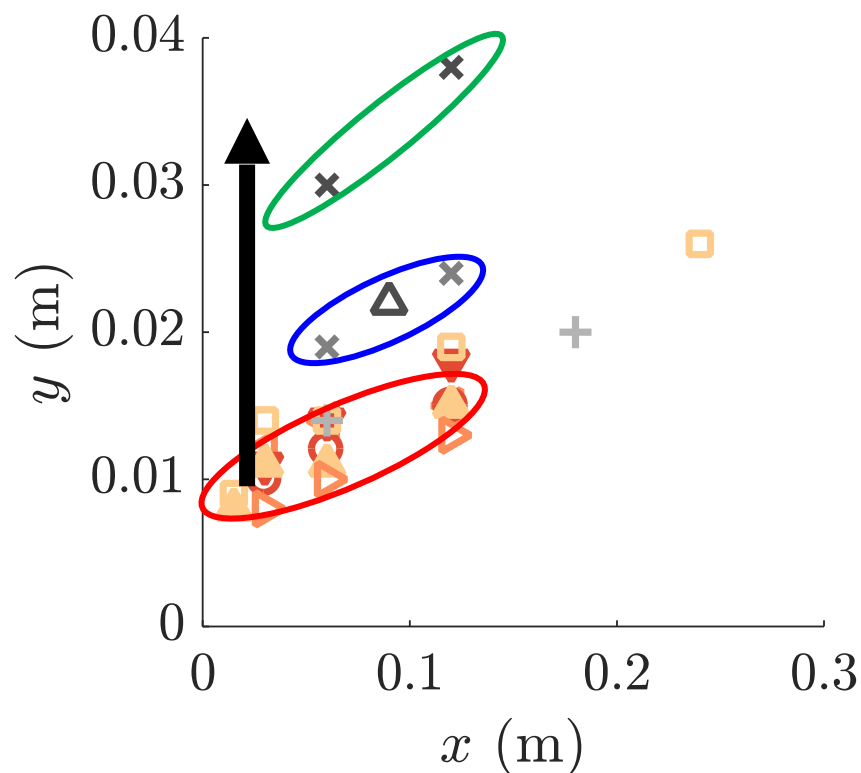
Results



Re_τ	r	$f\delta/U_\infty$	$f\nu/U_\tau^2$	fD/U_∞	
3200	0.3	1.8	0.016	13.0	▲
6350	0.3	1.8	0.008	13.6	▶
6350	0.3	1.8	0.009	6.2	◀
12800	0.3	2.3	0.004	6.8	▼
3200	0.3	1.0	0.009	6.9	◻
6350	0.3	1.8	0.008	13.6	◀
6350	0.3	1.8	0.009	6.2	◀
12800	0.3	4.1	0.010	16.2	○
3200	0.6	1.8	0.016	13.0	×
3200	0.9	1.8	0.016	13.0	×
6350	0.45	1.8	0.008	13.6	+
3200	0.9	5.4	0.049	39.0	△

A wide range of cases over variation in Reynolds number, frequency and velocity ratio

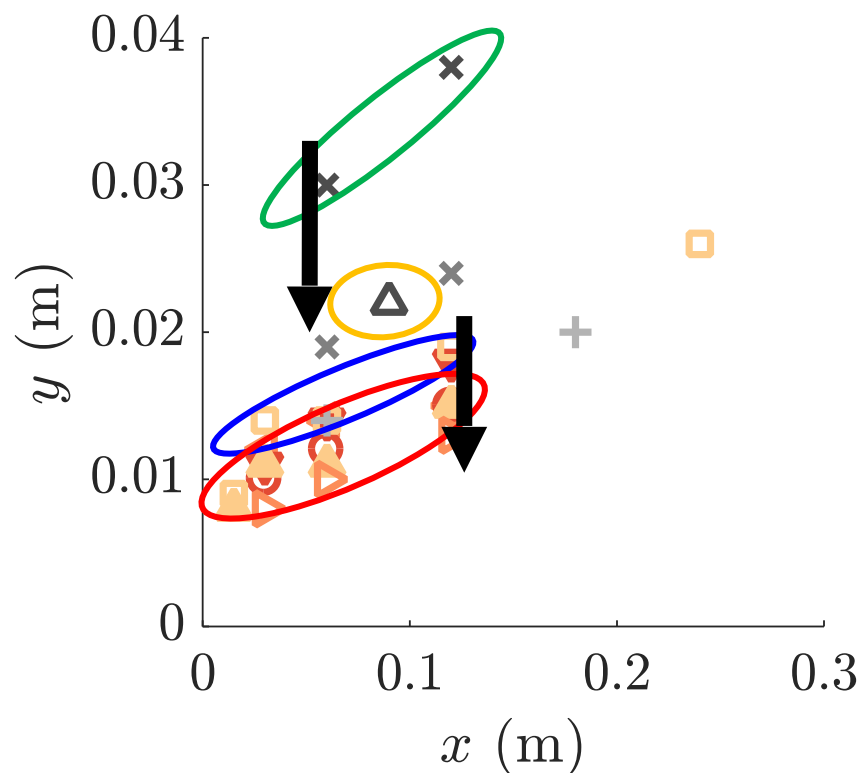
Effect of velocity ratio



Re_τ	r	$f\delta/U_\infty$	$f\nu/U_\tau^2$	fD/U_∞	
3200	0.3	1.8	0.016	13.0	▲
6350	0.3	1.8	0.008	13.6	▶
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12800	0.3	4.1	0.010	16.2	◉
3200	0.6	1.8	0.016	13.0	×
3200	0.9	1.8	0.016	13.0	×
6350	0.45	1.8	0.008	13.6	+
3200	0.9	5.4	0.049	39.0	△

Wall-normal penetration increases
with velocity ratio

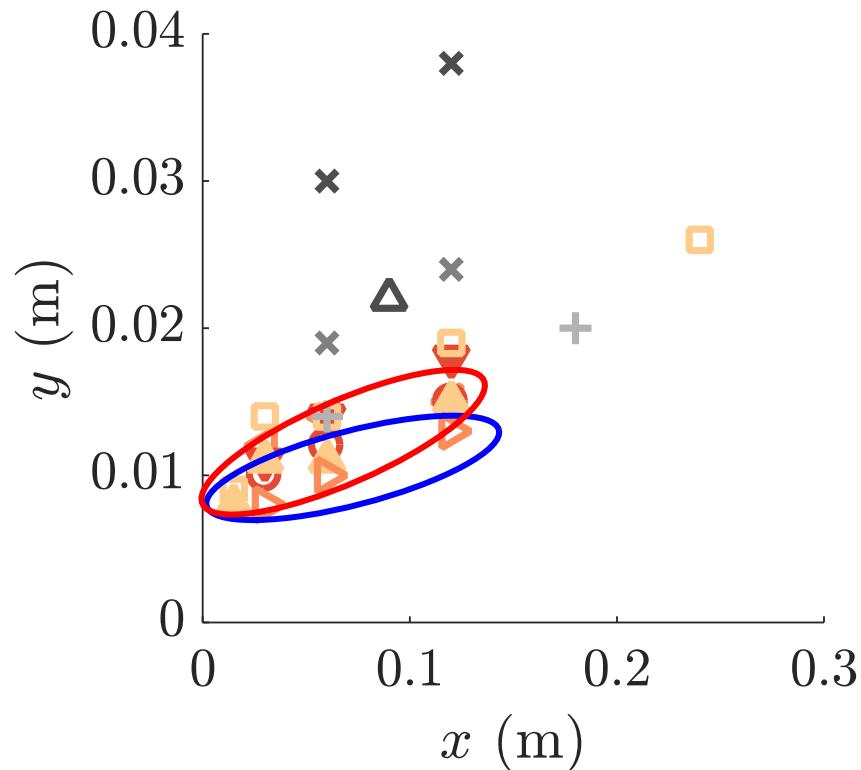
Effect of frequency



Re_τ	r	$f\delta/U_\infty$	$f\nu/U_\tau^2$	fD/U_∞	
3200	0.3	1.8	0.016	13.0	▲
6350	0.3	1.8	0.008	13.6	▶
6350	0.3	1.8	0.009	6.2	◀
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3200	0.9	1.8	0.016	13.0	×
6350	0.45	1.8	0.008	13.6	+
3200	0.9	5.4	0.049	39.0	△

Wall-normal penetration decreases
with frequency

Effect of Reynolds number

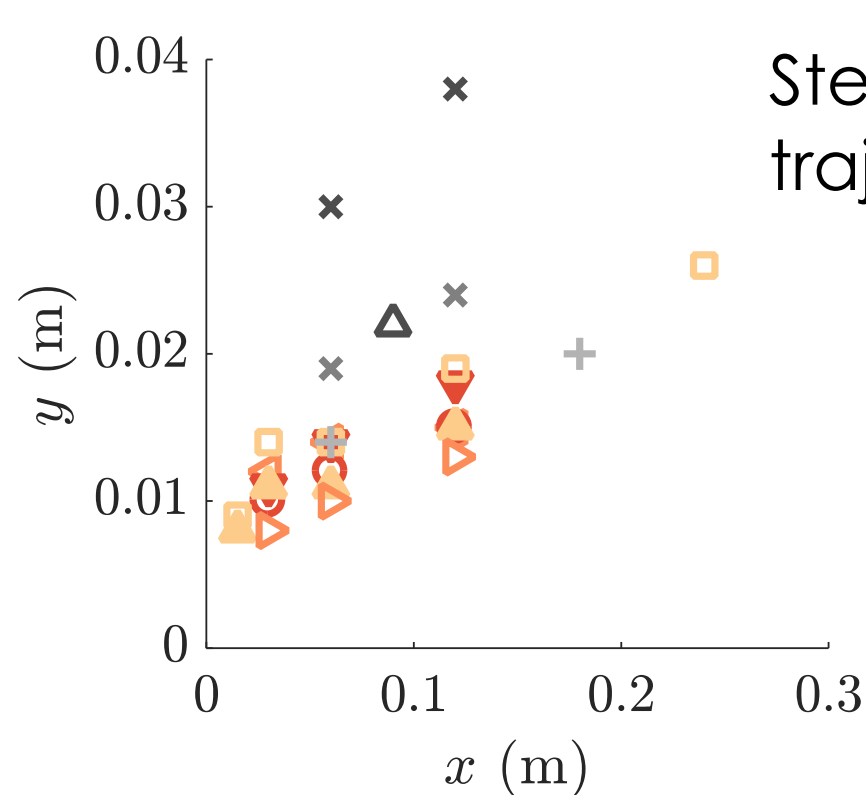


↓

Re_τ	r	$f\delta/U_\infty$	$f\nu/U_\tau^2$	fD/U_∞	
3200	0.3	1.8	0.016	13.0	▲
6350	0.3	1.8	0.008	13.6	▶
6350	0.3	1.8	0.009	6.2	◀
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6350	0.45	1.8	0.008	13.6	+
3200	0.9	5.4	0.049	39.0	▲

Reynolds number has a
minor effect on trajectory

Jet trajectory: Empirical model



Steady-jet trajectory: $\frac{y/D}{r^c} = A \left(\frac{x/D}{r^c} \right)^B$

$$\frac{y/D}{g(\dots)} = A \left(\frac{x/D}{g(\dots)} \right)^B$$

$$g(\dots) \propto \bar{U}^{c_1} f^{c_2} U_\infty^{c_3} \delta^{c_4}$$

Fit:

$$g(\dots) \propto \bar{U}^{1.2} f^{-0.6} U_\infty^{-0.8} \delta^{-0.1}$$

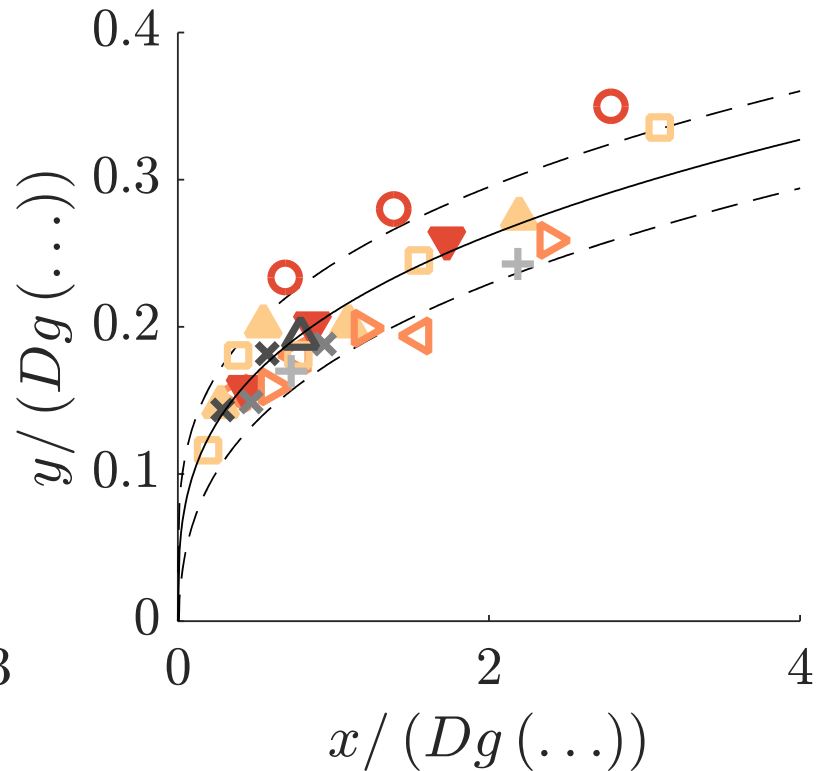
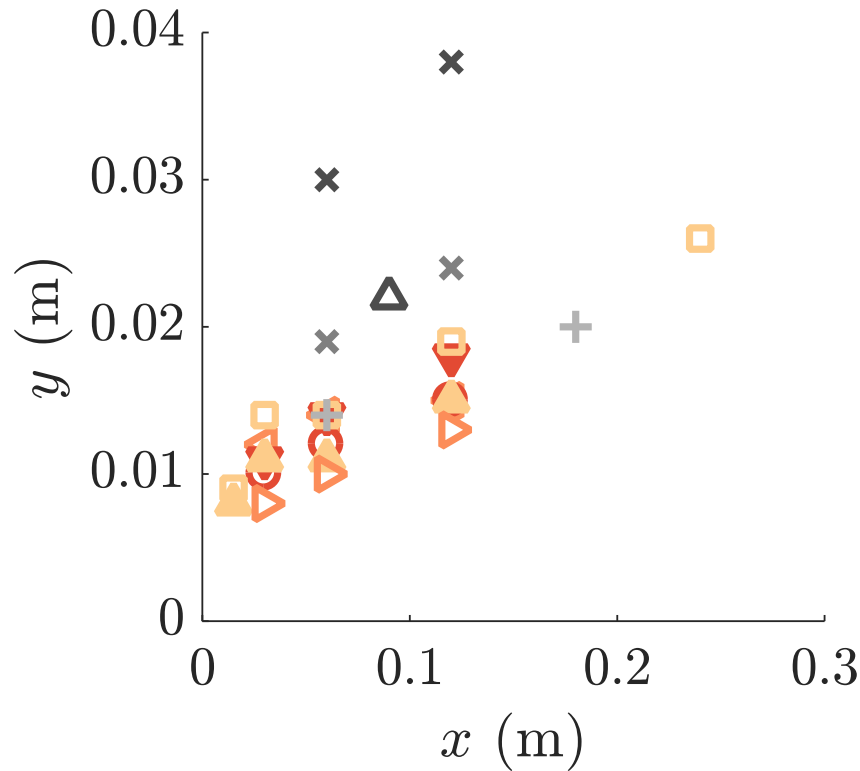
$$g(\dots) \propto r^{1.2} (U_\infty / (fD))^{0.6}$$

Velocity
scaling

Frequency
scaling

Reynolds number
scaling

Jet trajectory: Empirical model



$$\frac{y/D}{r^{1.2}(U_{\infty}/(fD))^{0.6}} = A \left(\frac{x/D}{r^{1.2}(U_{\infty}/(fD))^{0.6}} \right)^B$$

Jet trajectory: Empirical model

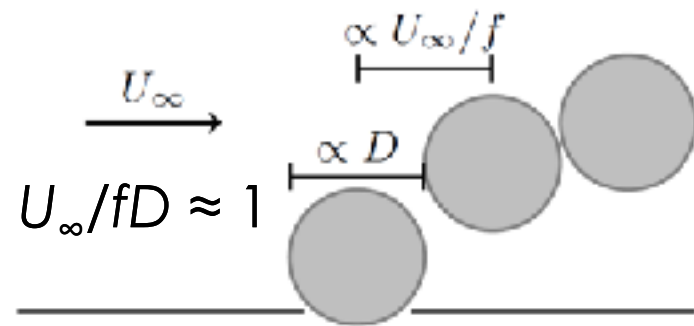
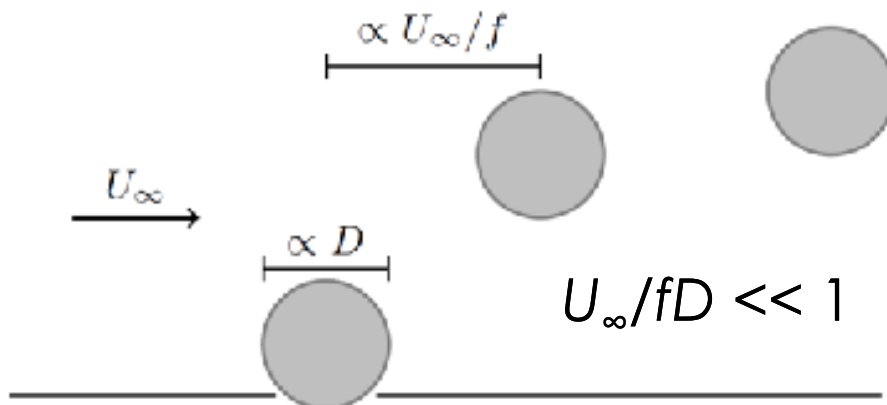
Synthetic-jet trajectory:

$$\frac{y/D}{r^{1.2} (U_{\infty}/(fD))^{0.6}} = A \left(\frac{x/D}{r^{1.2} (U_{\infty}/(fD))^{0.6}} \right)^B$$

Steady-jet trajectory:

$$\frac{y/D}{r^c} = A \left(\frac{x/D}{r^c} \right)^B$$

In the limit of a steady jet the original power-law scaling is recovered!



How does the jet strength decay with downstream distance?
We could explore this in moderate Reynolds number facilities

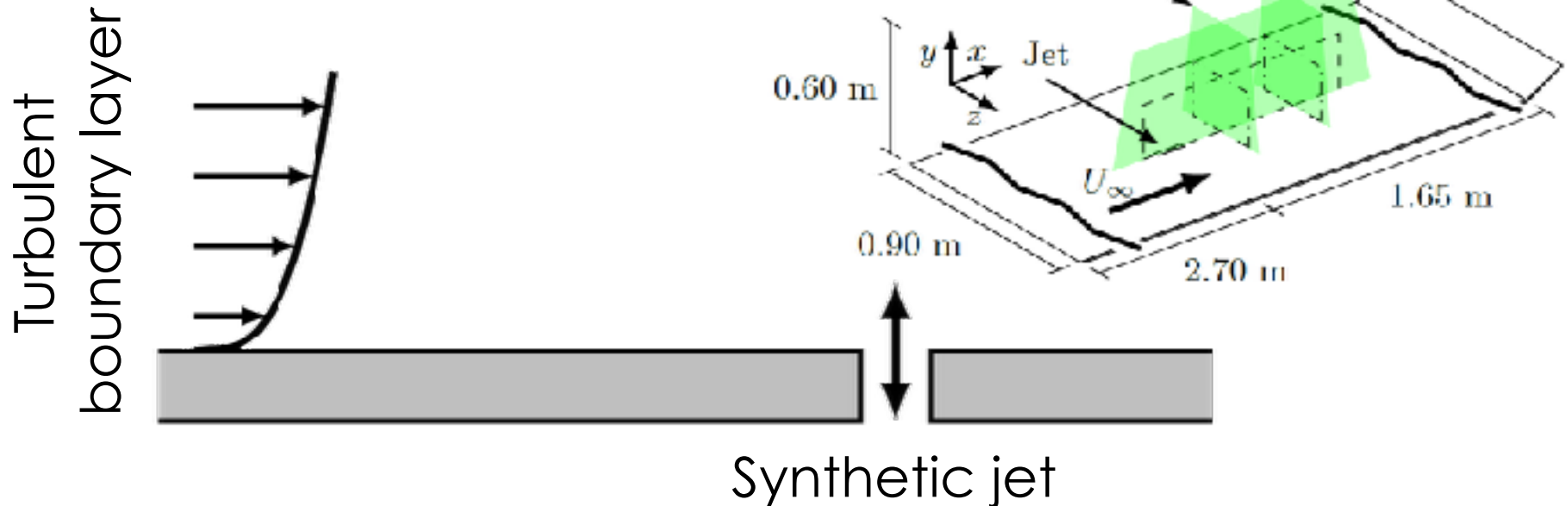
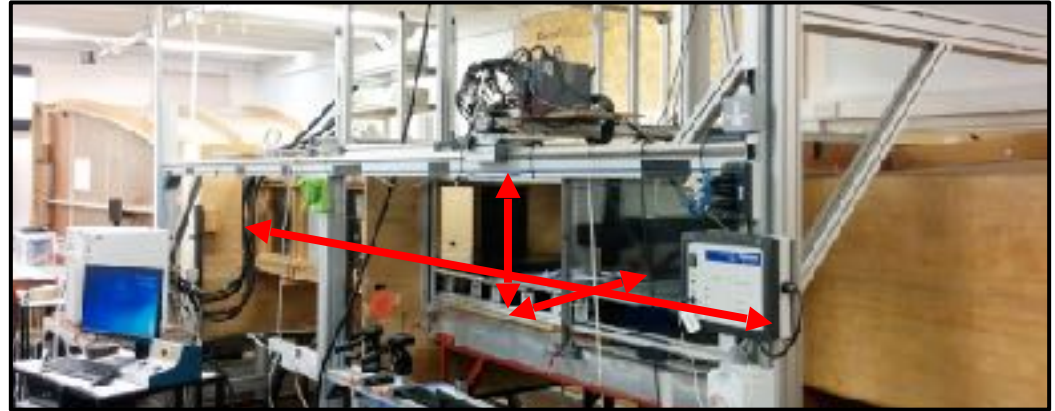
Jet decay: Facility

3' x 2' turbulent boundary layer wind tunnel

0.6 m x 0.9 m x 4.5 m

$Re_\tau = 1250$

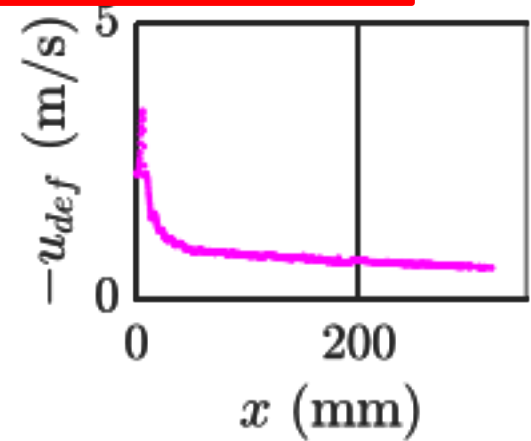
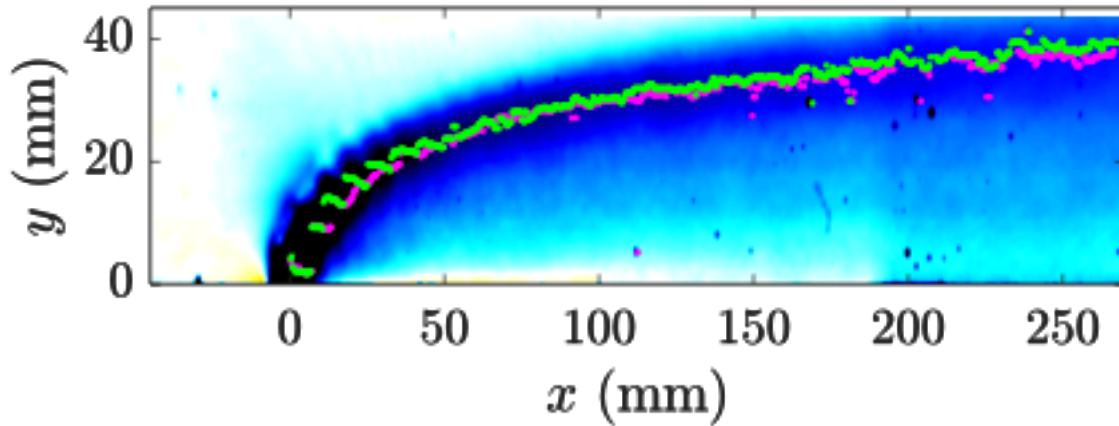
$\delta = 0.05$ m



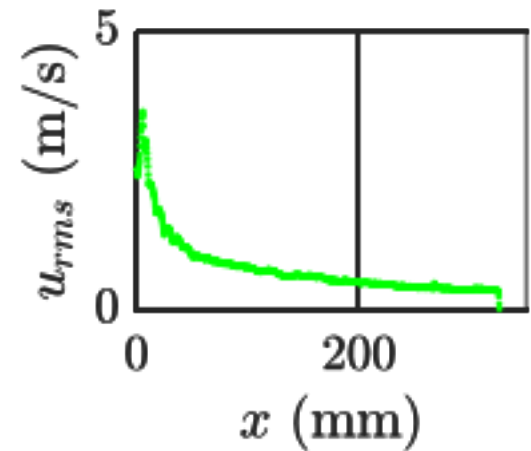
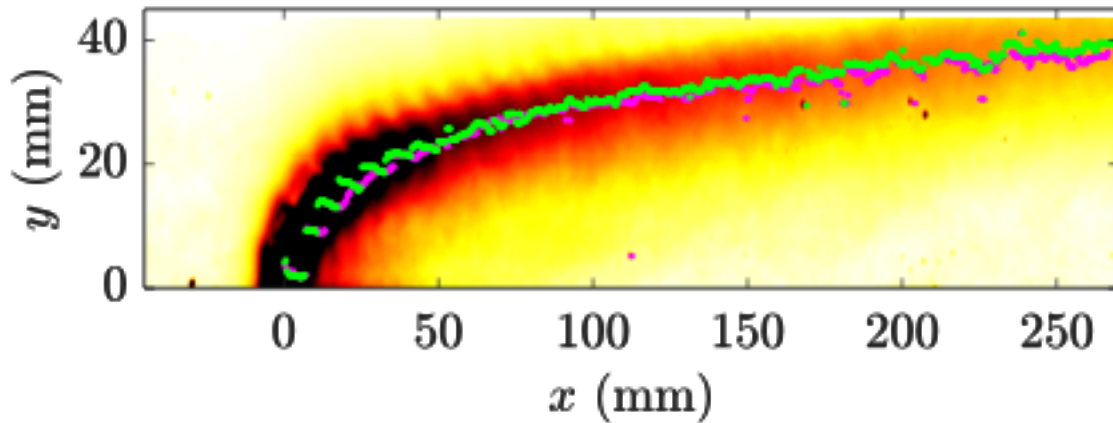
Jet decay

Velocity deficit:

Both methods give very similar results



Velocity rms:



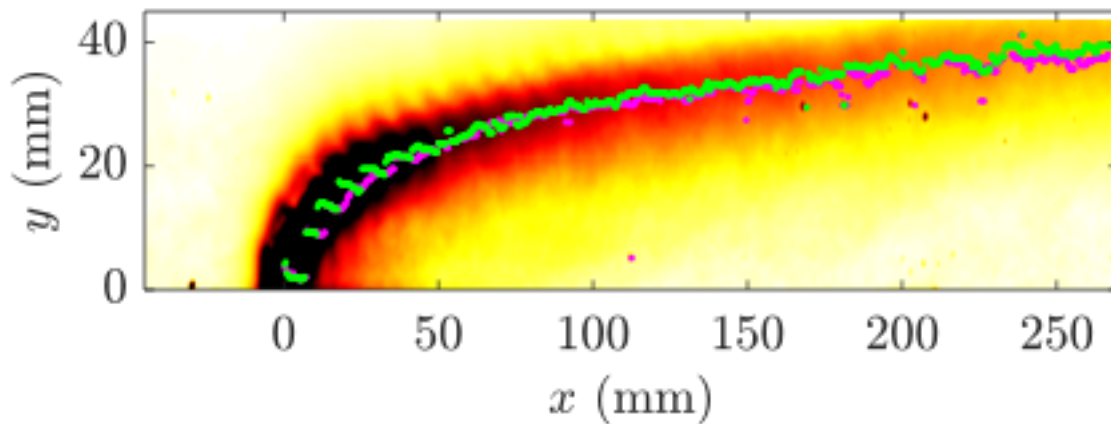
Jet decay

Velocity deficit:

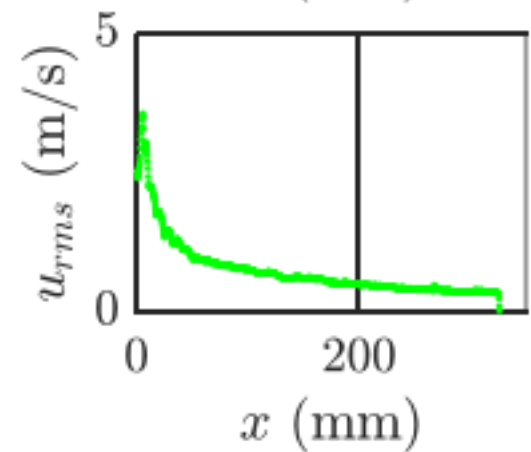
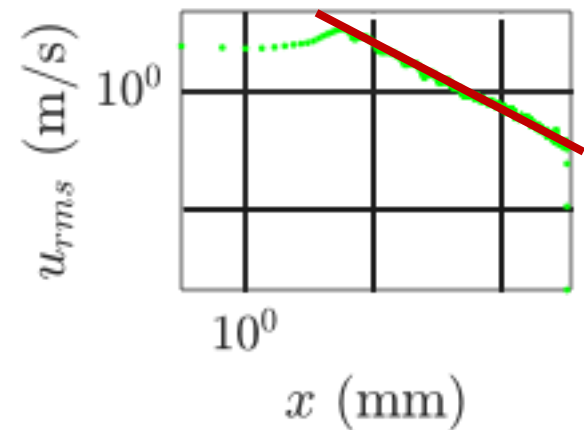
Both methods give very similar results

- RMS only depends on the local velocity signal
- The velocity deficit compares the perturbed with the unperturbed velocity, leading to larger uncertainties for hot-wire measurements

Velocity rms:

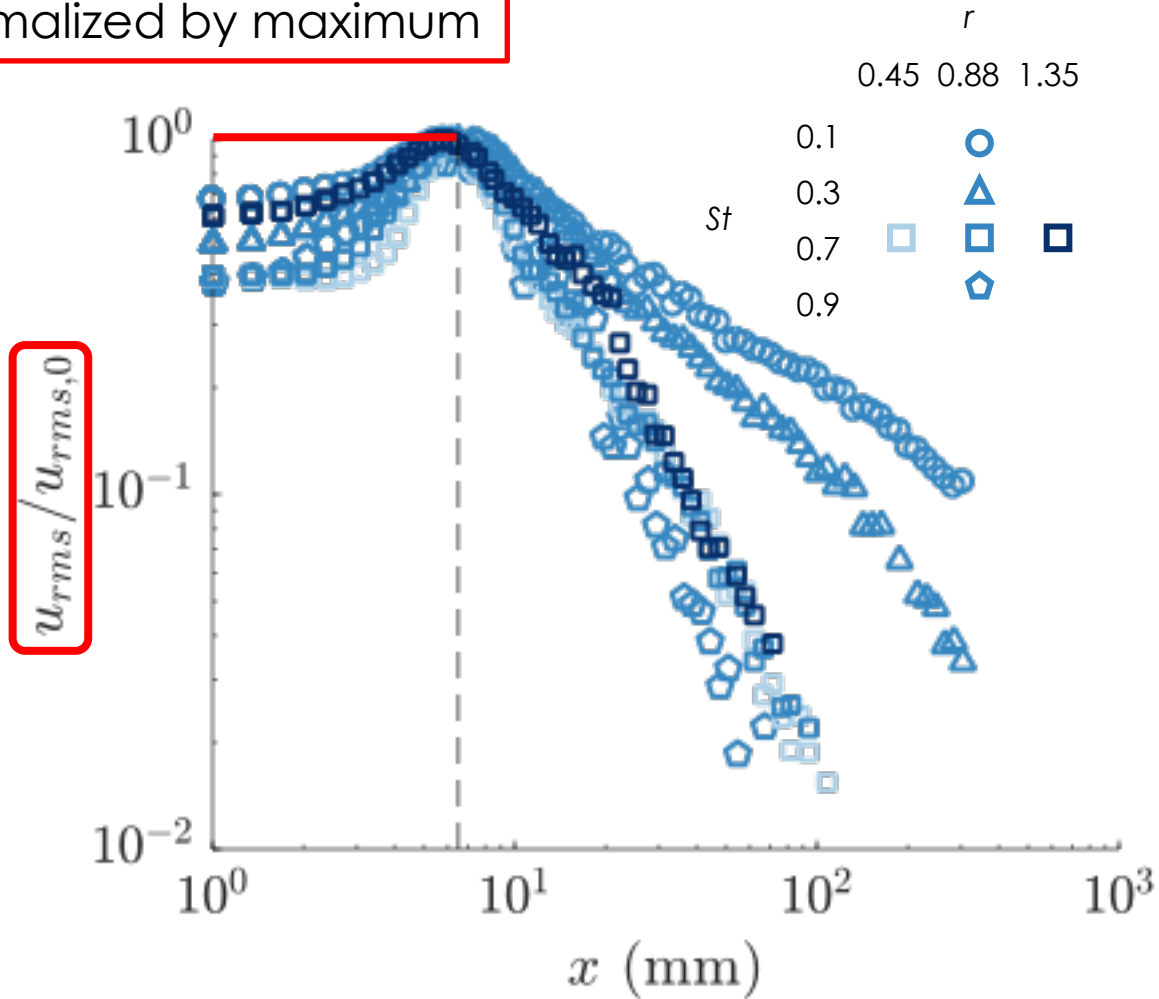


Power-Law decay



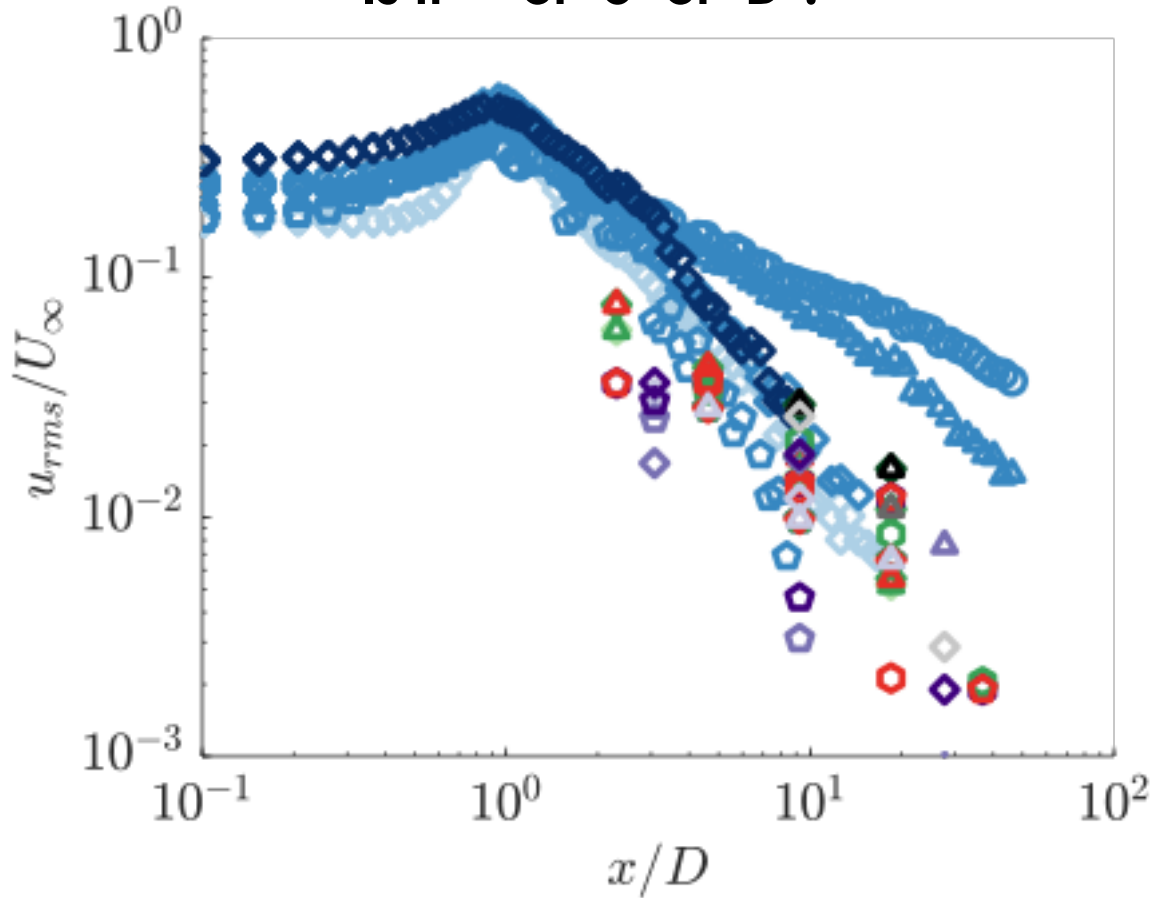
Jet decay

RMS is normalized by maximum



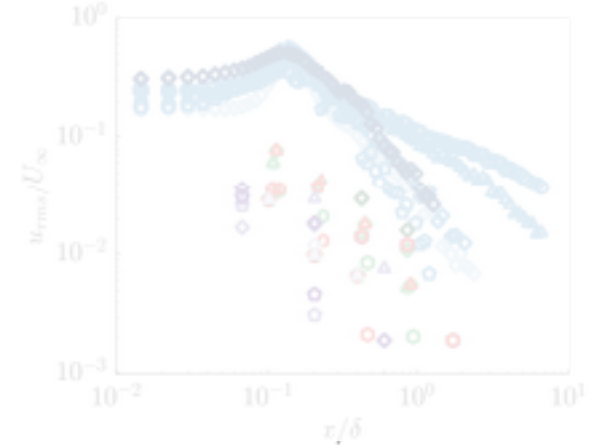
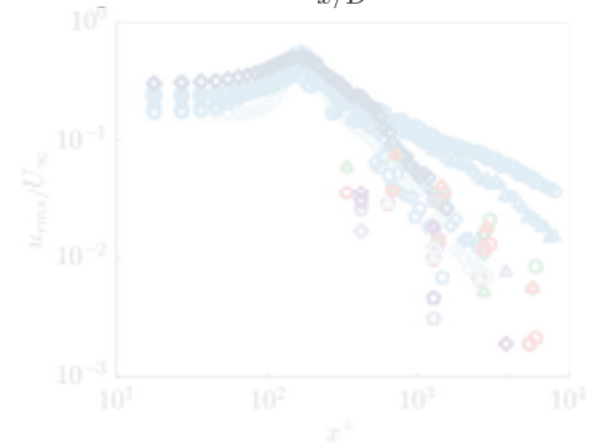
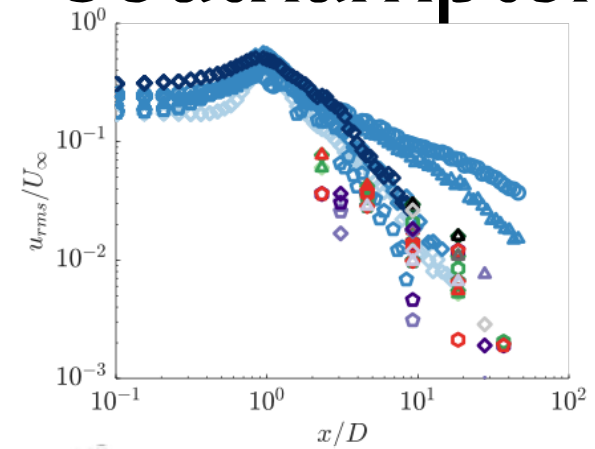
Jet decay

This data can be used to examine scaling:
Is it '+' or 'δ' or 'D'?



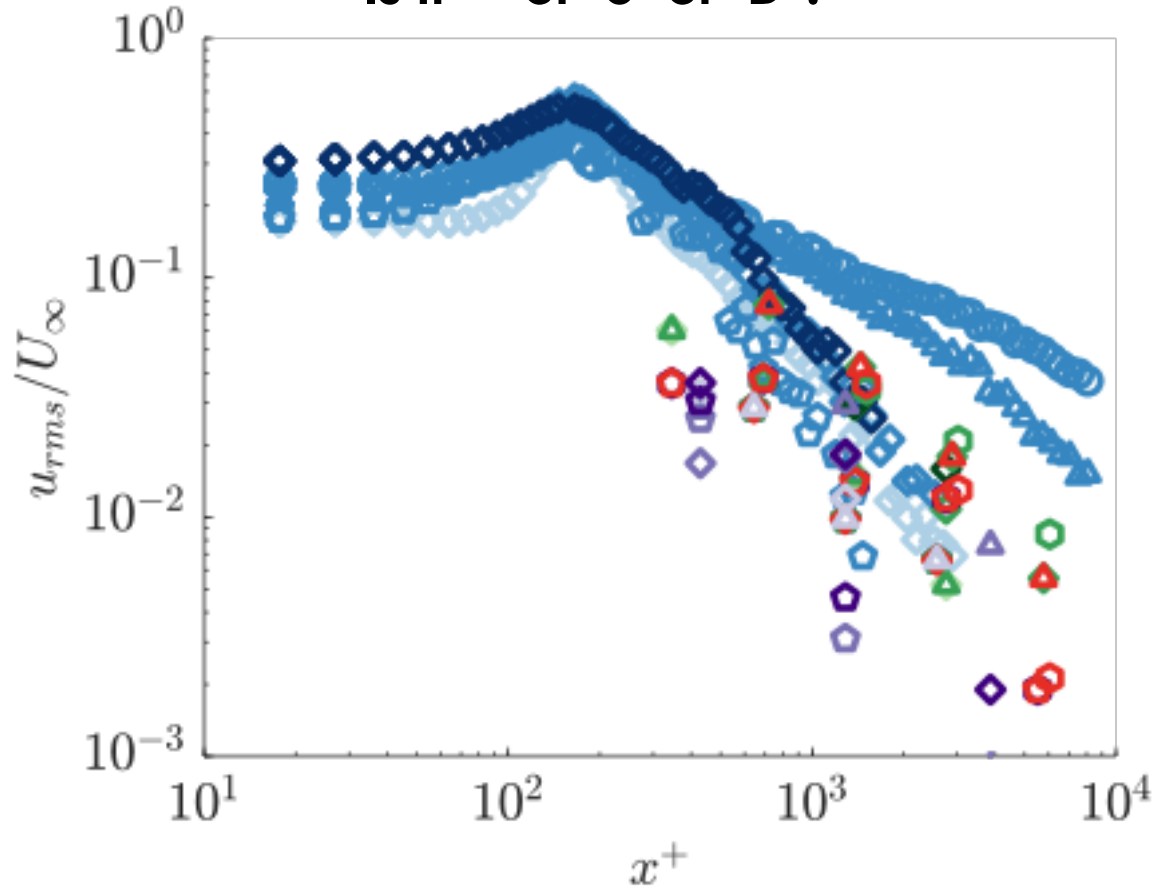
Reasonable collapse of jet decay

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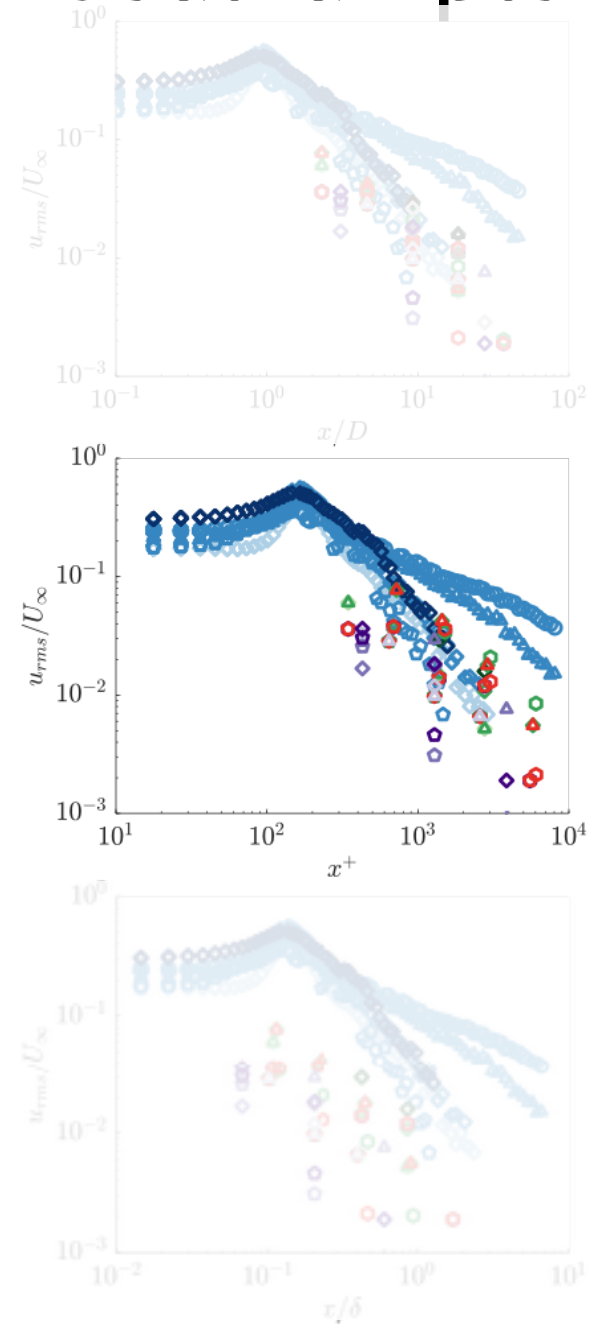


Jet decay

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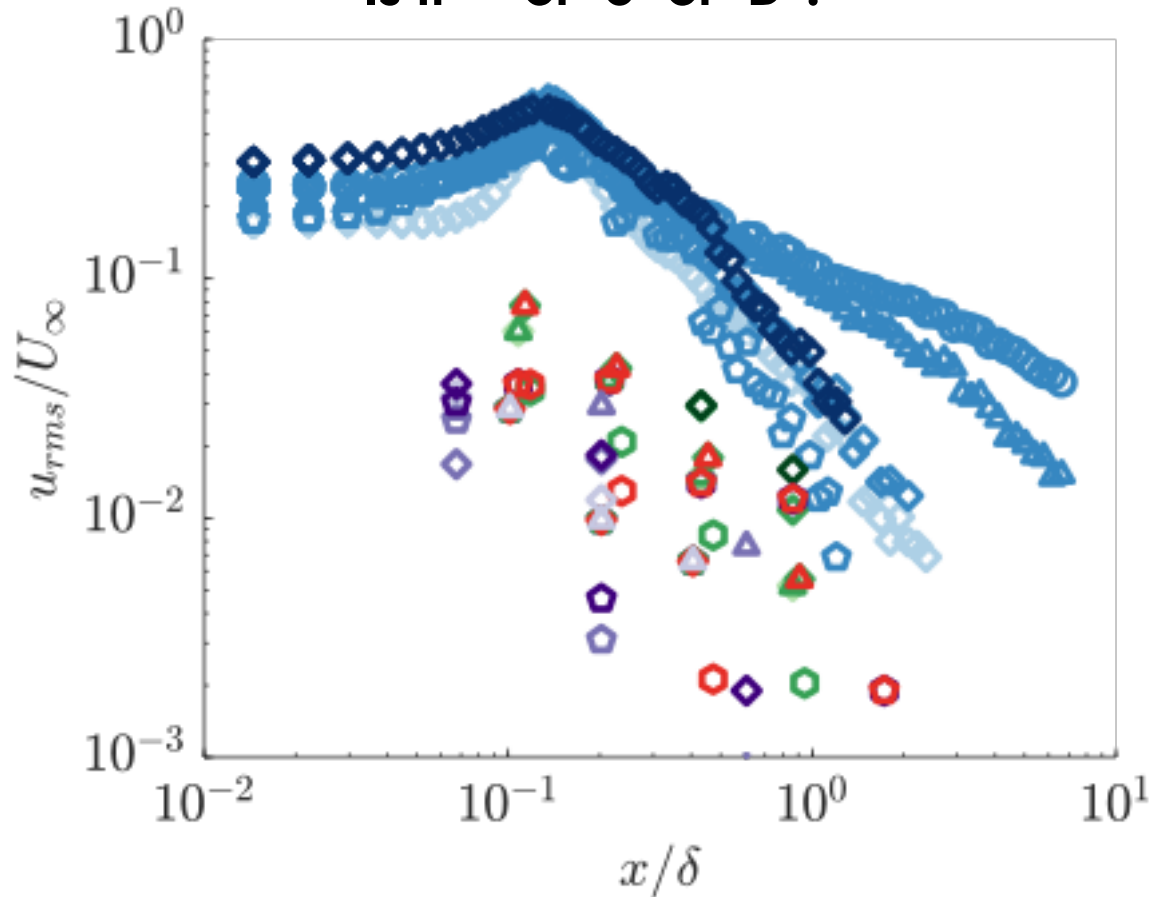


x^+ shows a slightly larger spread
of the data

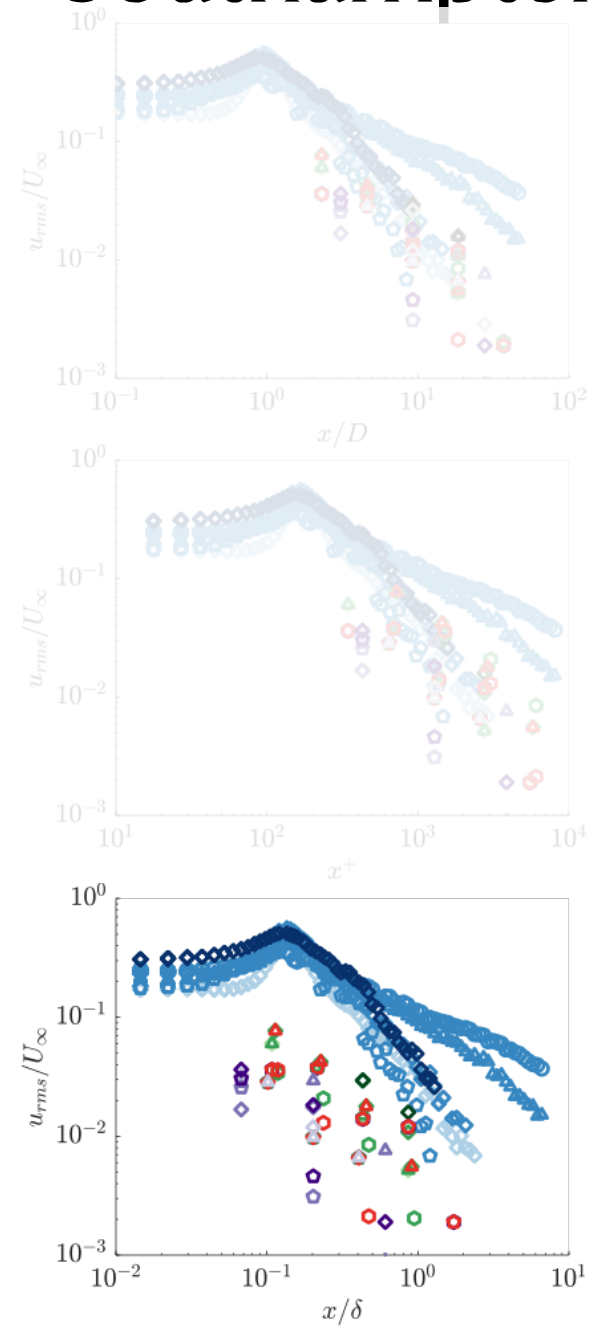


Jet decay

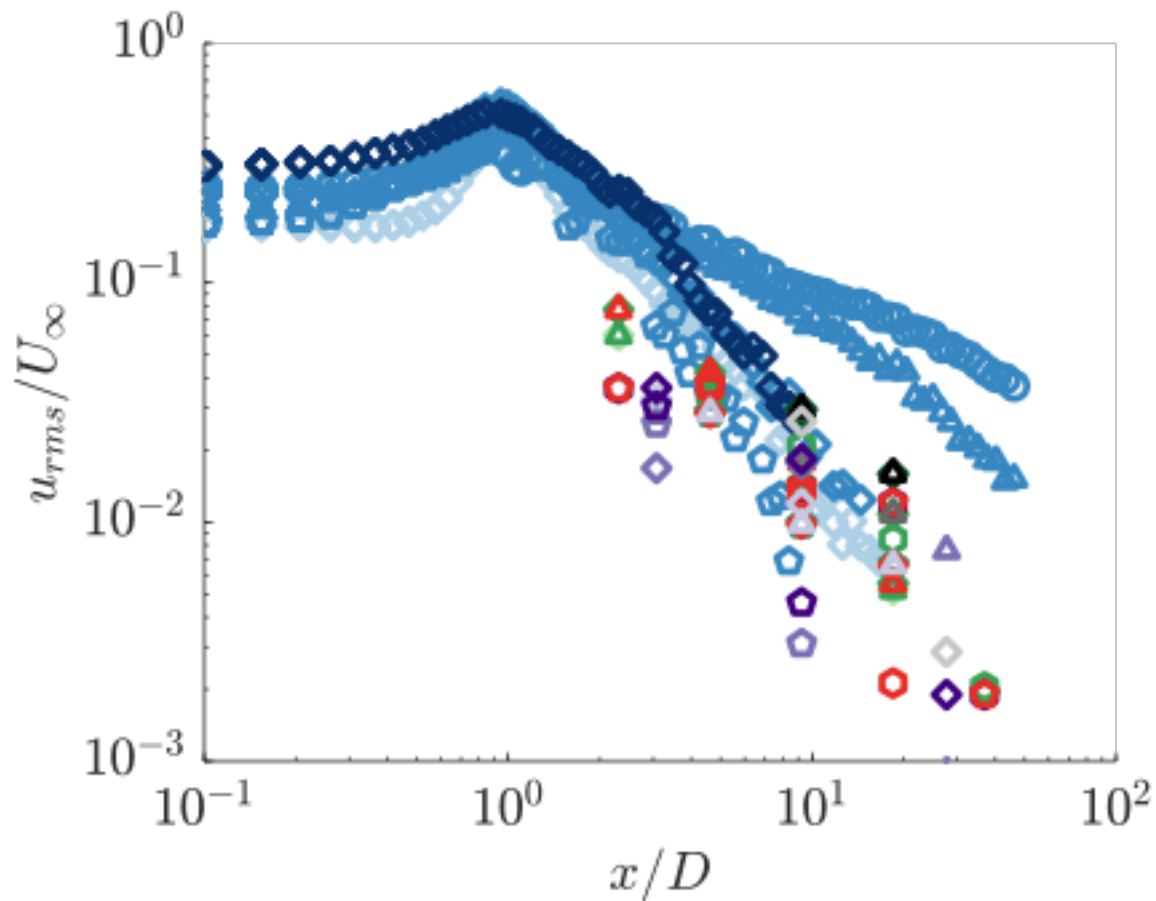
This data can be used to examine scaling:
Is it '+' or ' δ ' or 'D'?



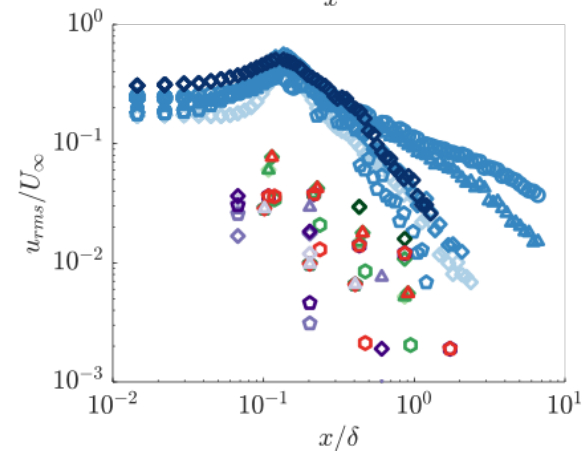
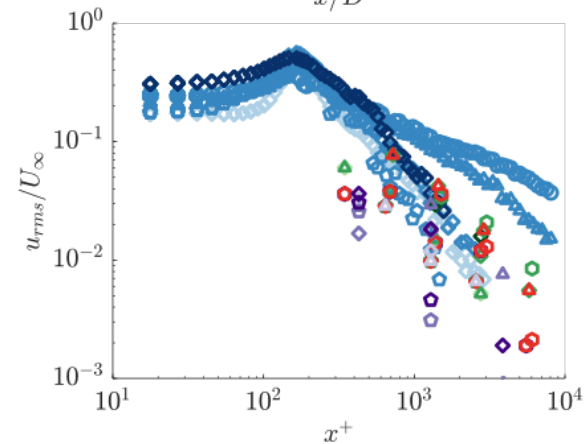
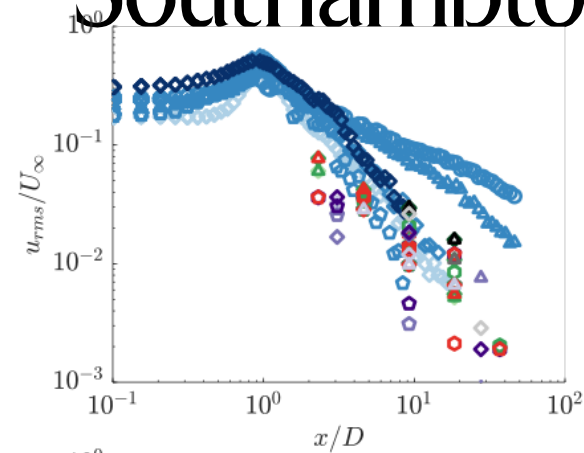
x/δ shows a much larger
spread of the data



But this data can be used to investigate scaling with ' x^+ ' or ' δ '

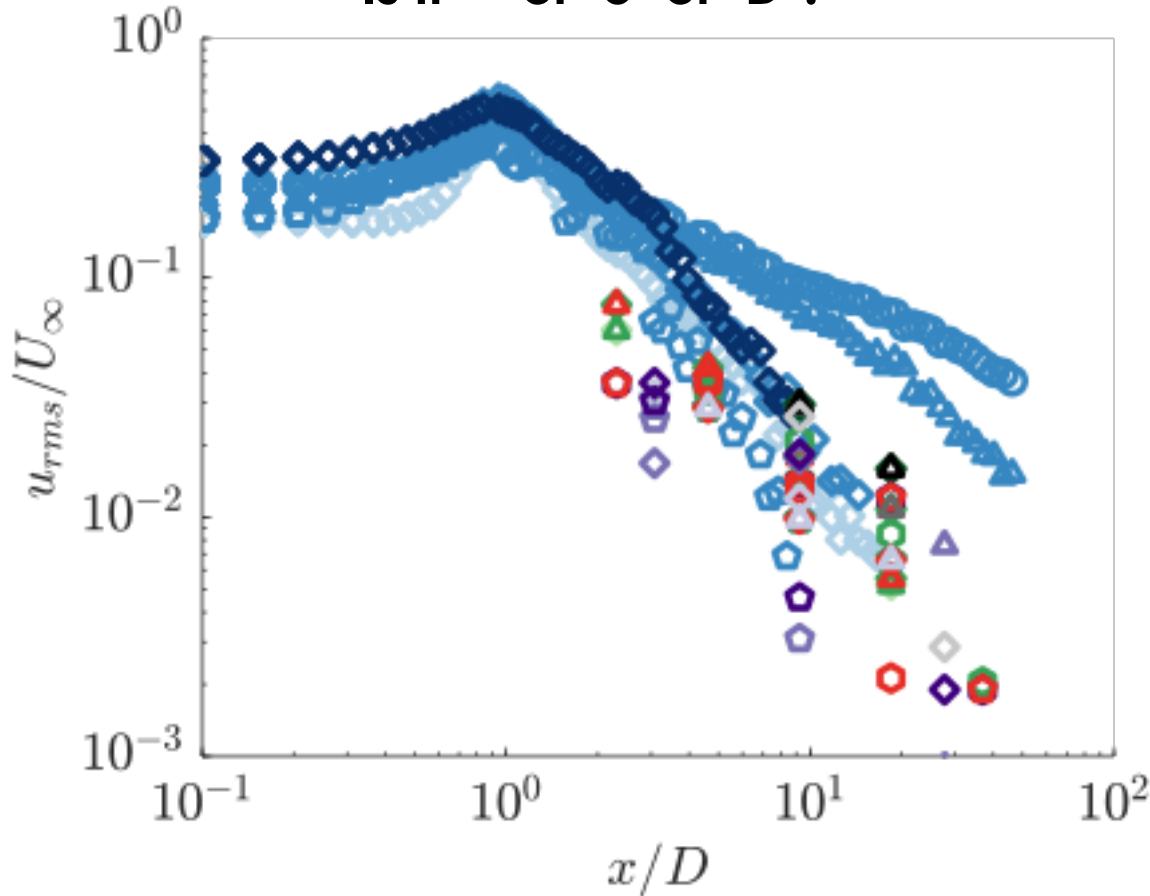


This suggests that neither x/δ nor x^+ should be used to scale the decay



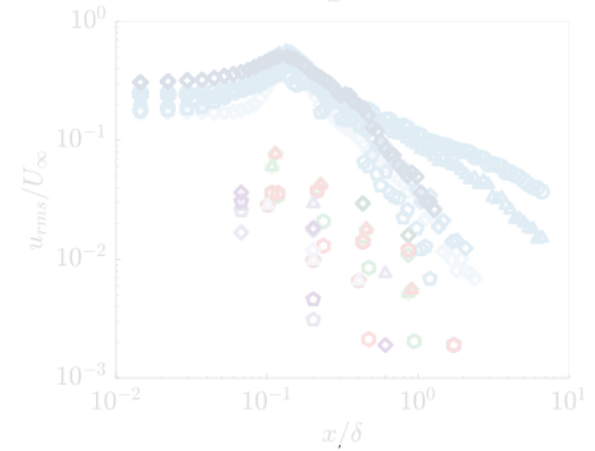
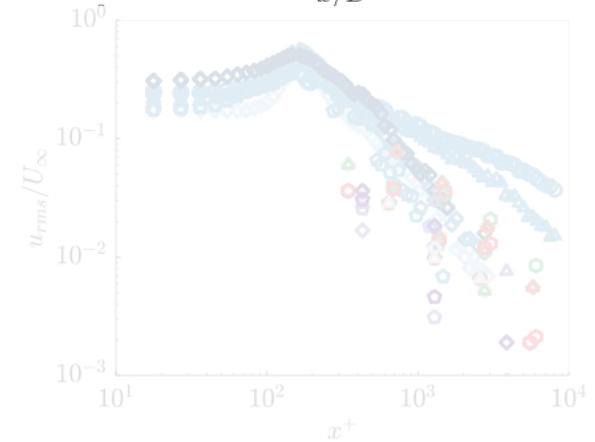
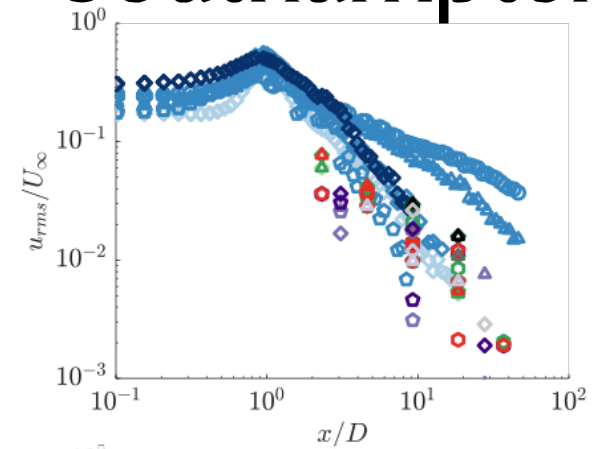
Jet decay

This data can be used to examine scaling:
Is it '+' or 'δ' or 'D'?

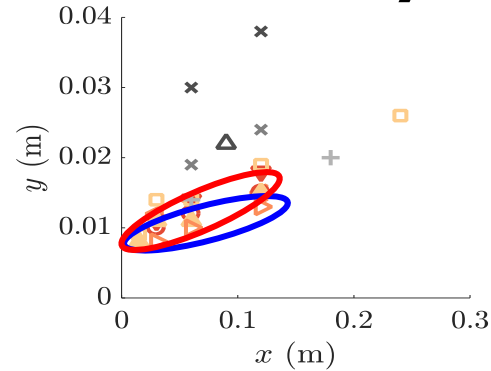


Reasonable collapse of jet decay
Consistent with free-wakes

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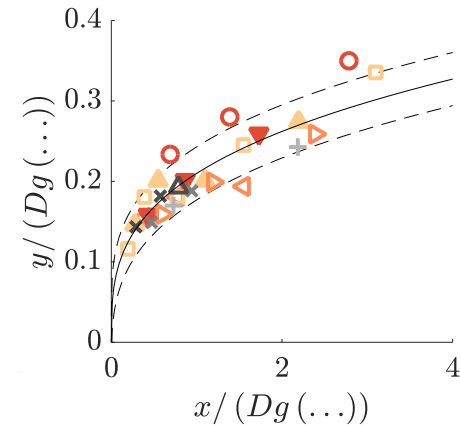
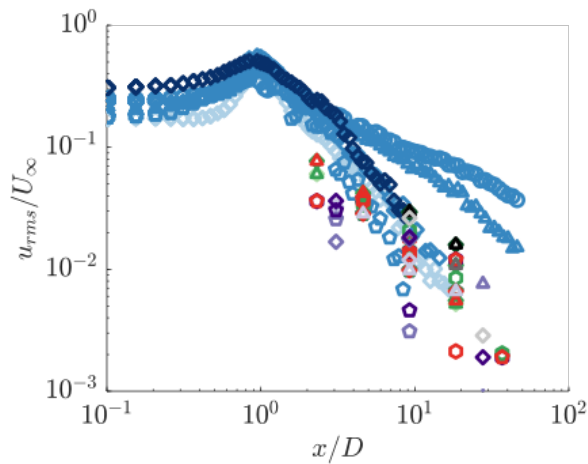


Summary



The Reynolds number only has a small influence on the trajectory of a synthetic jet

The jet trajectory follows a power-law for which an empirical scaling has been derived



Jet decay appears to scale with jet dimensions

Actuator requirements for large-scale control?

Jet frequency determined by passage of VLSMs

Determine velocity ratio based on the derived empirical scaling for the trajectory

Location of subsequent jets along streamwise direction scales with jet dimensions

Thank you!

www.bharath-lab.org

g.bharath@soton.ac.uk