

# Experimental Investigations of Active Control of a Turbulent Boundary Layer for Skin Friction Drag Reduction

Airbus/SIG Workshop

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Dec 5, 2017



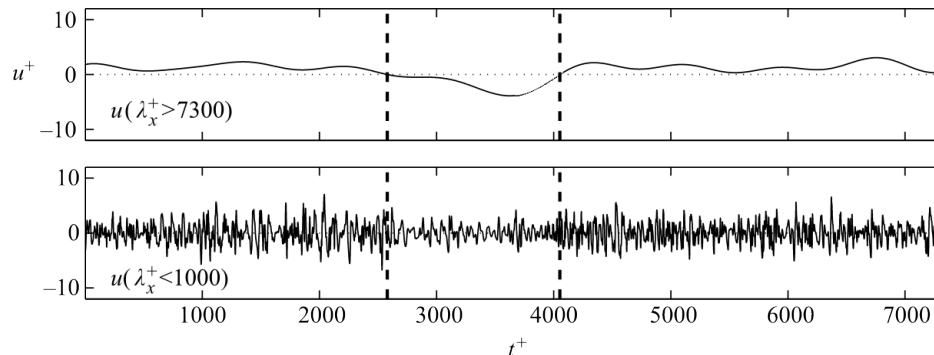
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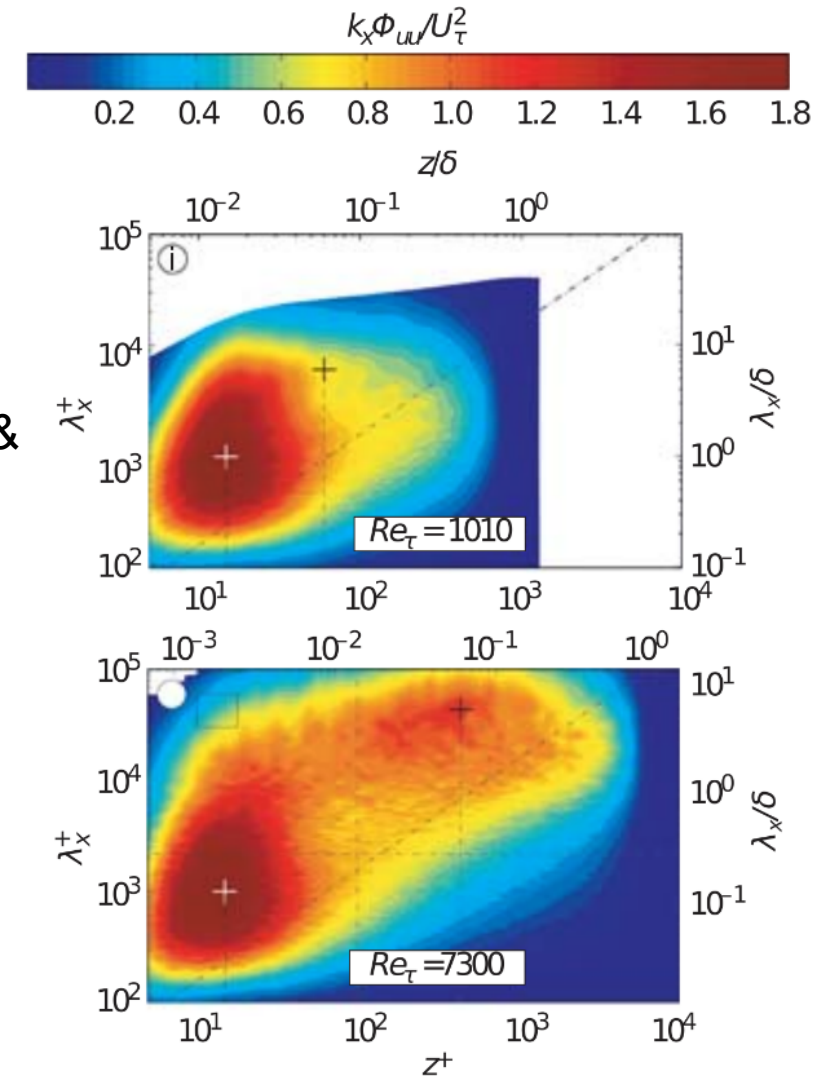
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# Introduction

- Control skin-friction drag in a TBL:
  - Target turbulence production in near wall cycle
    - Small length and time scales
    - Riblets (e.g. Walsh 1983), oscillating wall (e.g. Choi 1998), etc.
  - Target large scale coherent structures in the log region
    - Shown to have a modulation effect on near wall cycle (Hutchins & Marusic 2007b)
    - Contain increasingly larger fraction of TKE as Re increased
    - Continuous jets (Abbasi 2017), wall deformation (e.g. Bai 2014), etc.
- We use synthetic jets to attempt to affect large scale structures in a TBL with a goal of reducing skin-friction



Hutchins & Marusic 2007b



Hutchins & Marusic 2007a

# Wind Tunnel and Flow Characteristics

Flow characteristics:

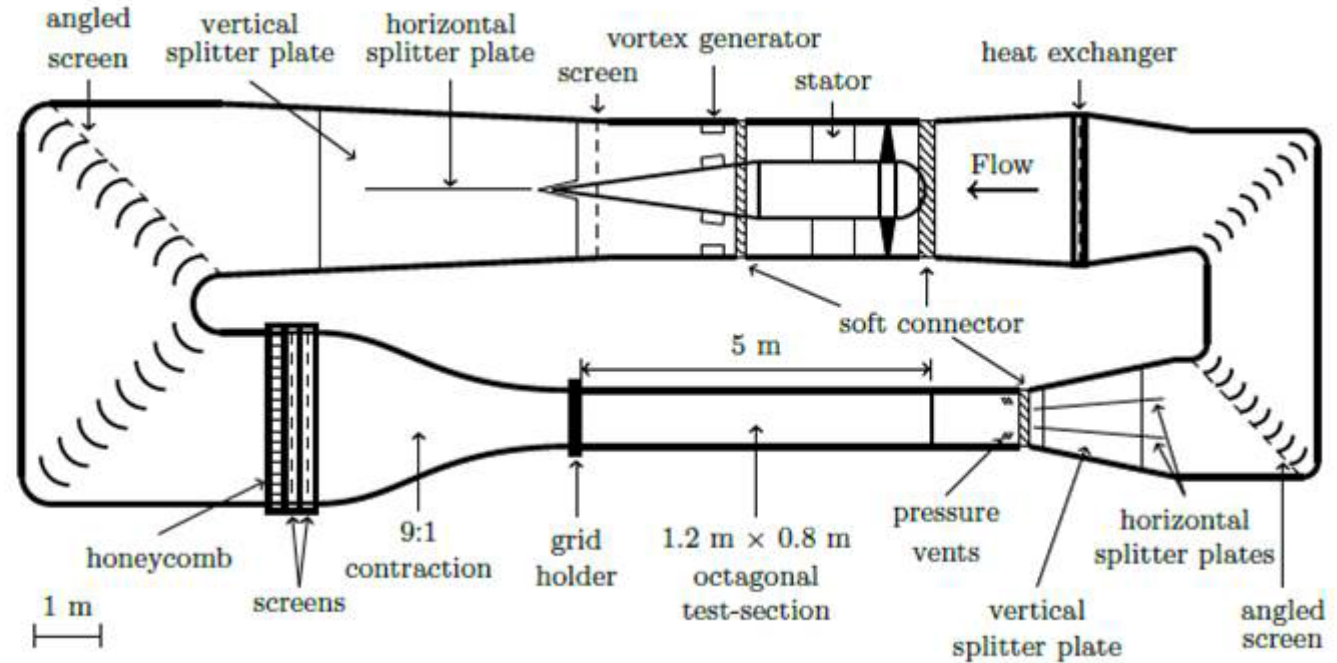
$U_\infty$	$\delta$	$\delta^*$	$\theta$	$H$	$U_\tau$	$c_f$	$Re_\theta$	$Re_\tau$
10.01 m/s	42.5 mm	7.19 mm	5.16 mm	1.395	0.401 m/s	0.0032	3200	1070

$$Re_\theta = \frac{\theta U_\infty}{\nu}$$

$$Re_\tau = \frac{\delta U_\tau}{\nu}$$

$$U_\tau = \sqrt{\nu \left. \frac{\partial u}{\partial x} \right|_w}$$

$$c_f = 2 \left( \frac{U_\tau}{U_\infty} \right)^2$$



# Wind Tunnel and Flow Characteristics

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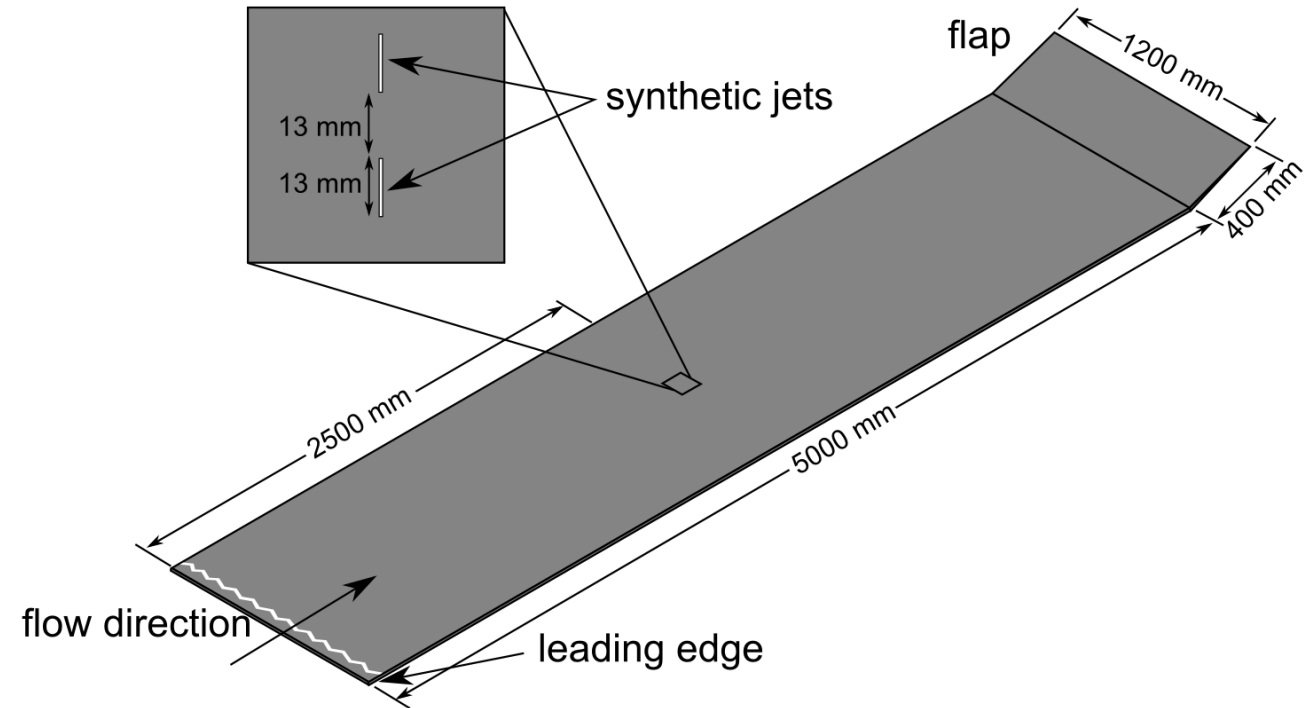
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# Synthetic Jets

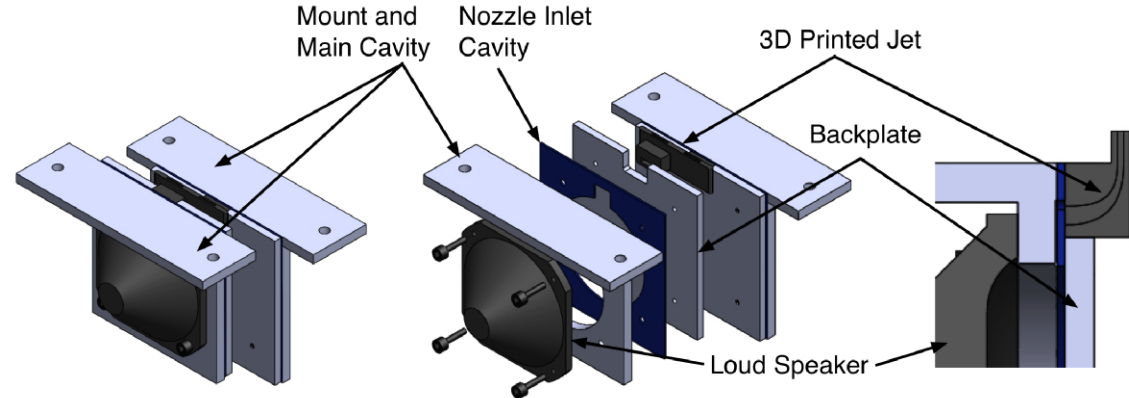
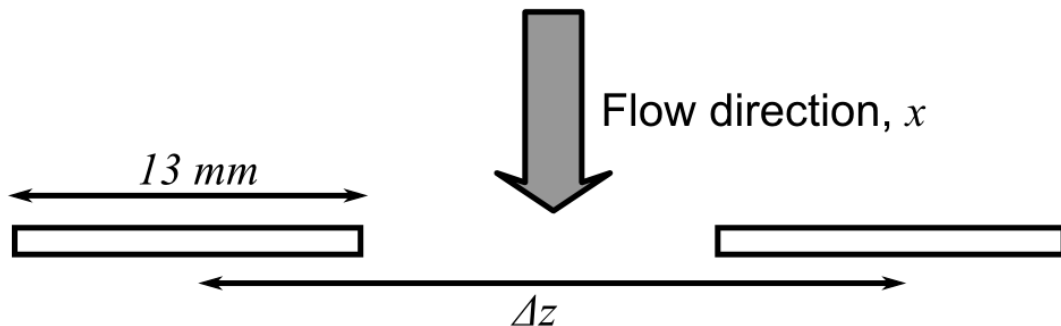
## Parameters:

Strouhal number,  $St = \frac{f\delta}{U_\infty}$

Blowing ratio,  $r = \frac{U_j}{U_\infty}$

where  $U_j = \frac{1}{T} \int_0^{T/2} u_j(t) dt$

Jet Spacing,  $\Delta z / \delta$

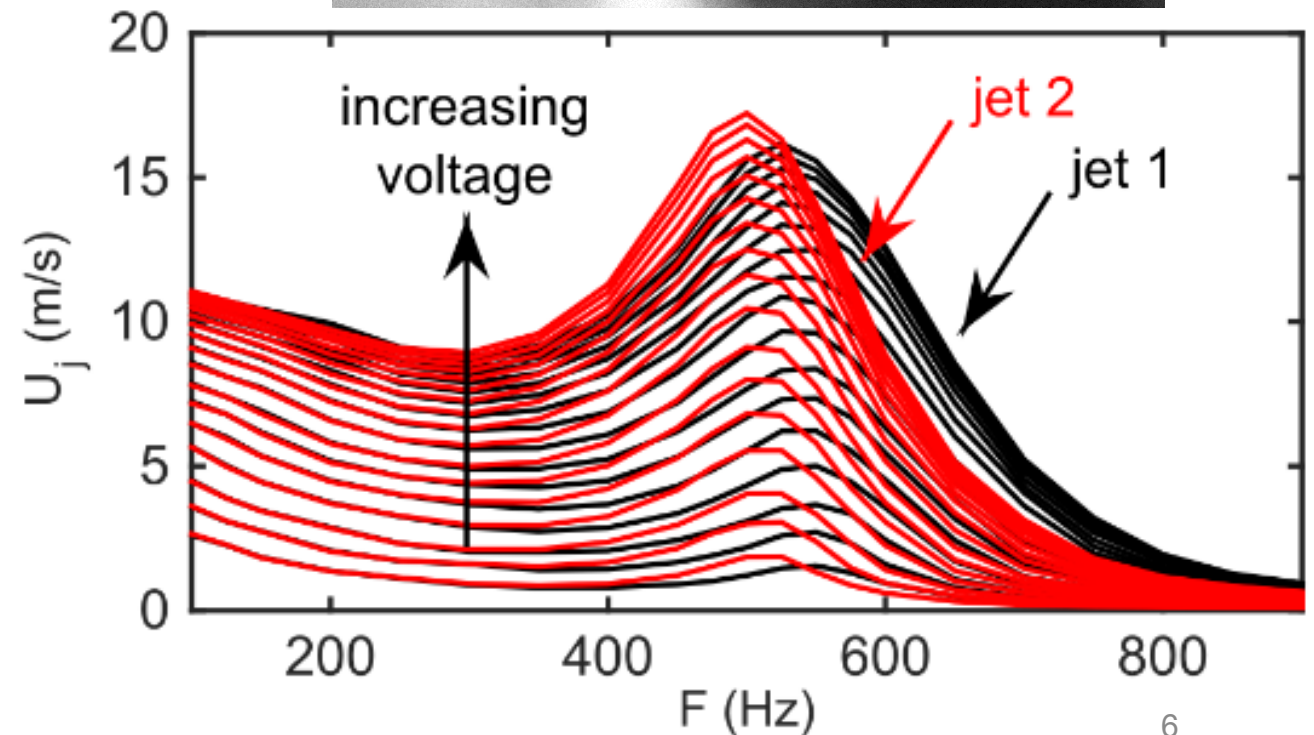
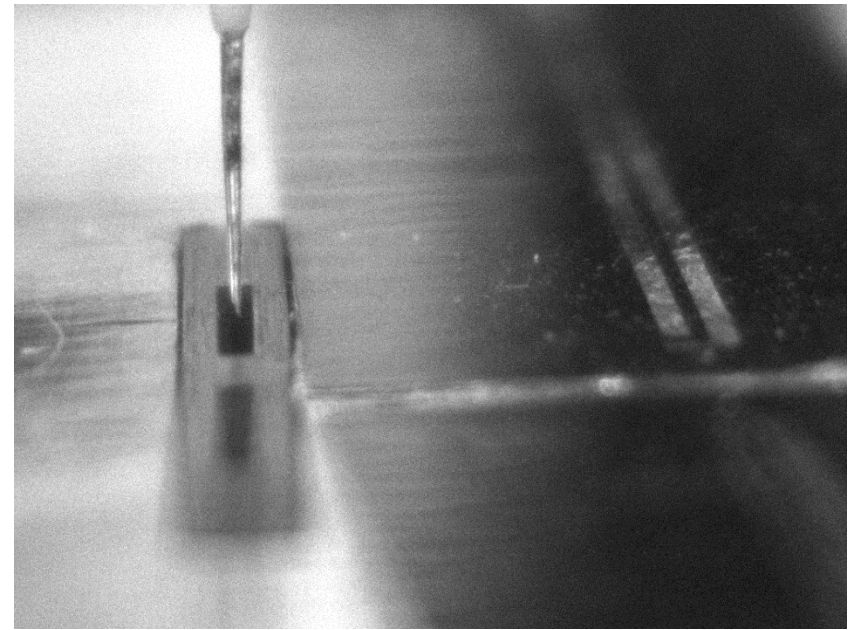


- Size of jet orifice slots chosen to match large scale structures in the log region
- Spanwise extent of structures is approx.  $0.2\delta - 0.3\delta$  (Ganapathisubramani (2005))
- At our experimental conditions, this results in a slot width of 13 mm.



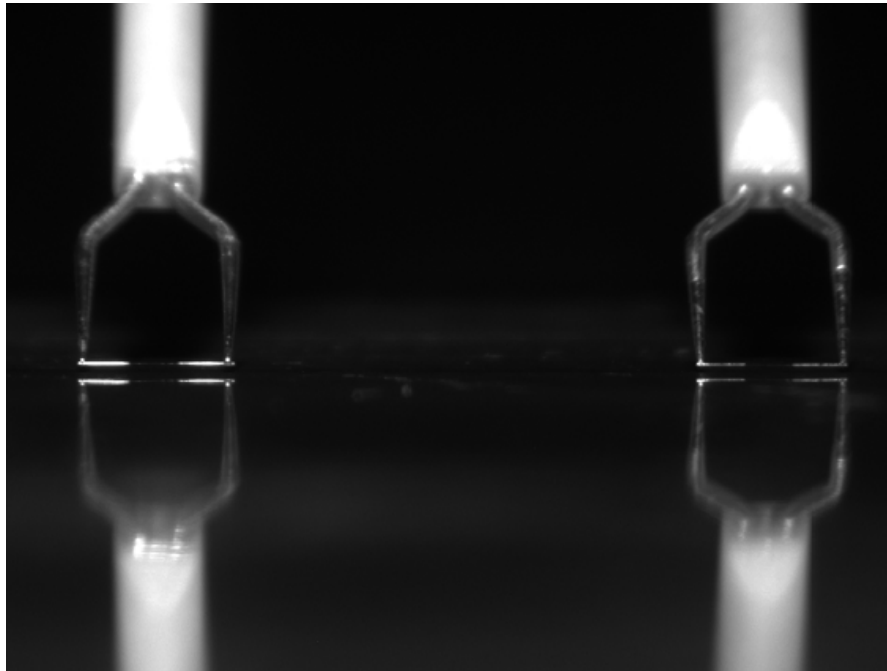
# Synthetic Jet Calibration

- Vary the frequency and voltage output by function generator to SJ speakers
- Hot wire at jet exit to measure jet velocity  $U_j$
- Do independently for each jet



# Hot Wire Measurements

- Two hot-wires spaced 13 mm apart in spanwise direction
- 5 cases investigated
  - Effect of Strouhal number
  - Effect of blowing ratio



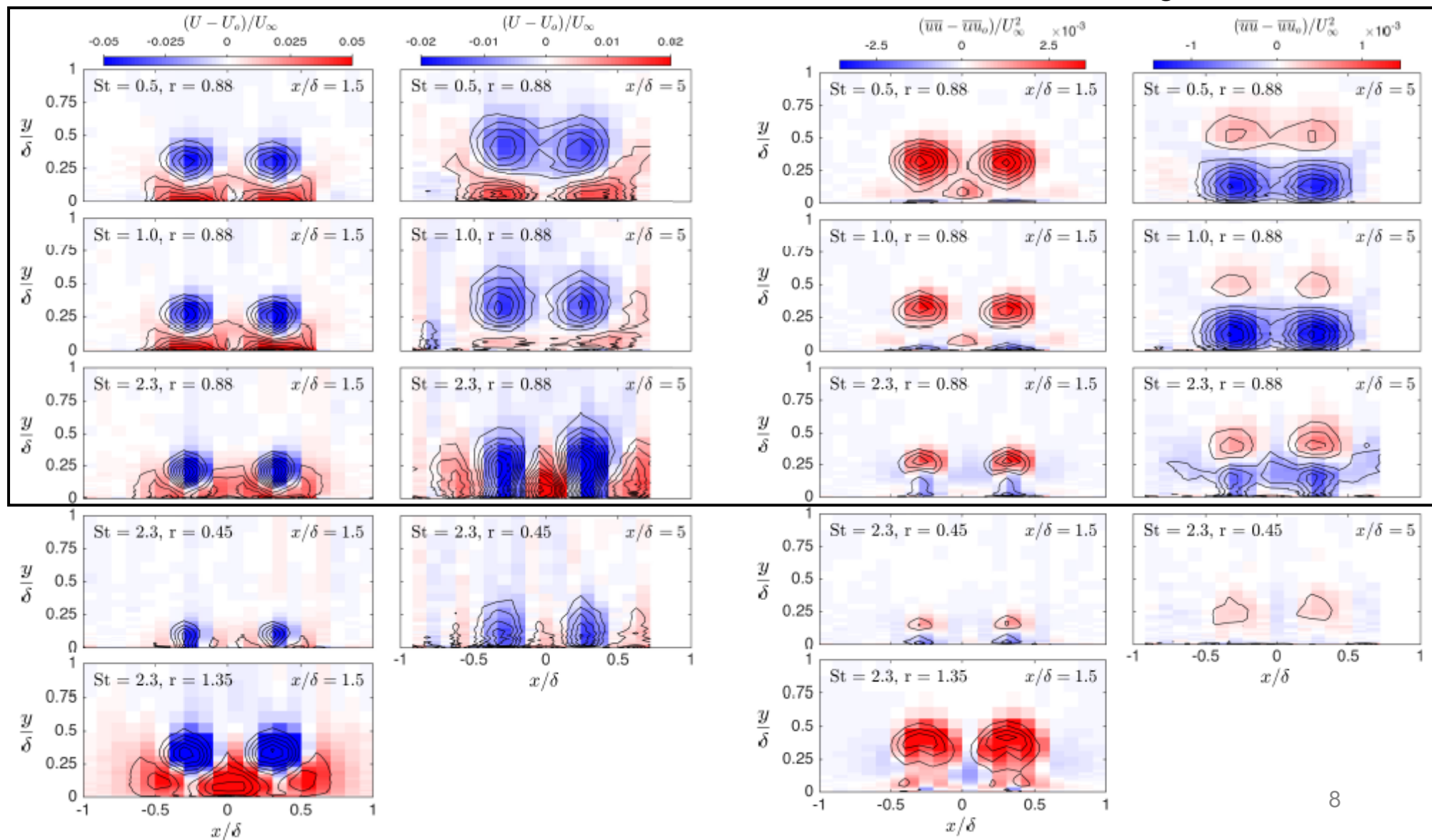
Case	(Hz)	$U_j$ (m/s)	$St$	$r$
1	119	8.8	0.5	0.88
2	238	8.8	1.0	0.88
3	548	8.8	2.3	0.88
4	548	4.5	2.3	0.45
5	548	13.5	2.3	1.35

# Effect of Jets on Mean Flow

Mean

Fluctuating

Constant  $r$   
Increasing  $St$

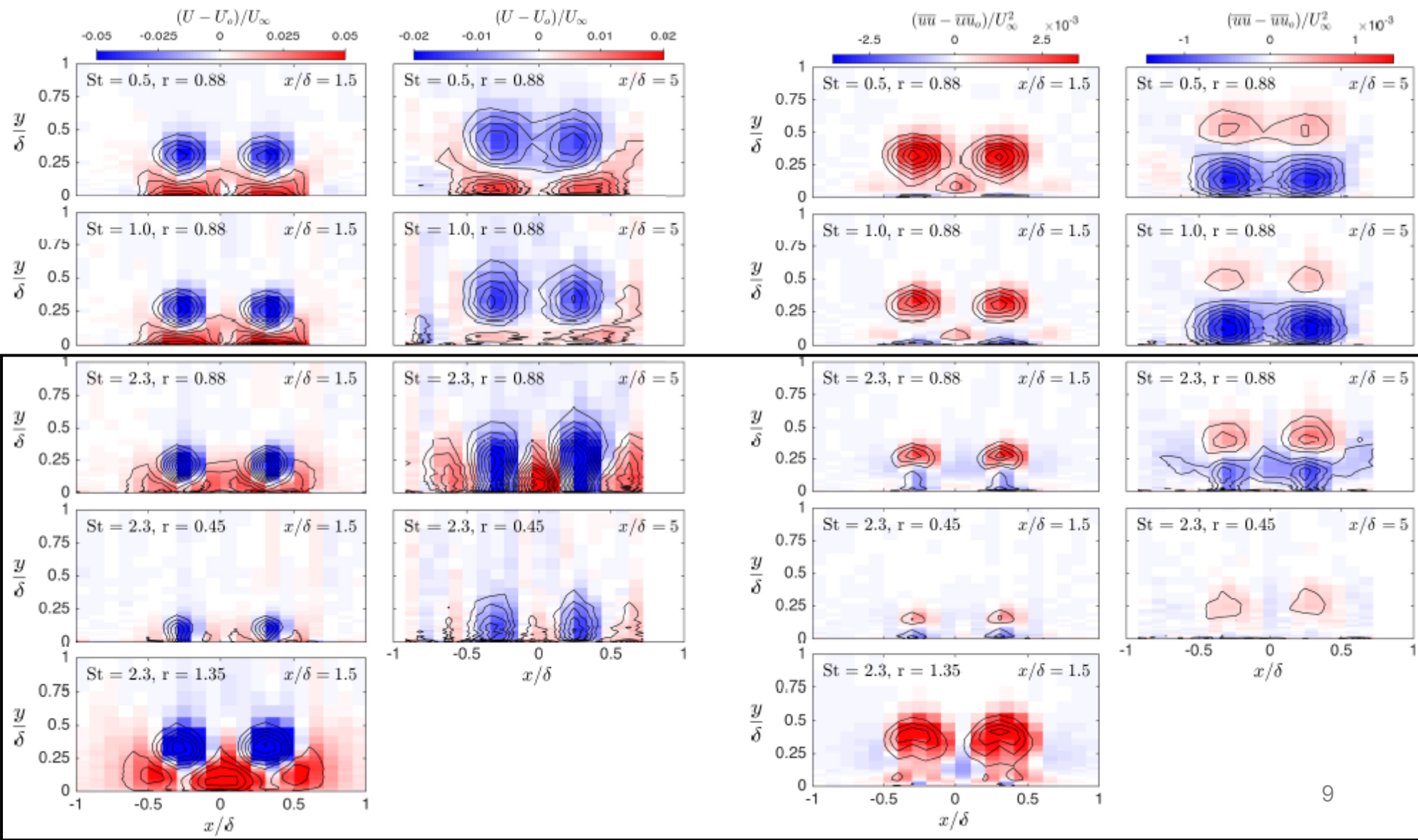




# Effect of Jets on Mean Flow

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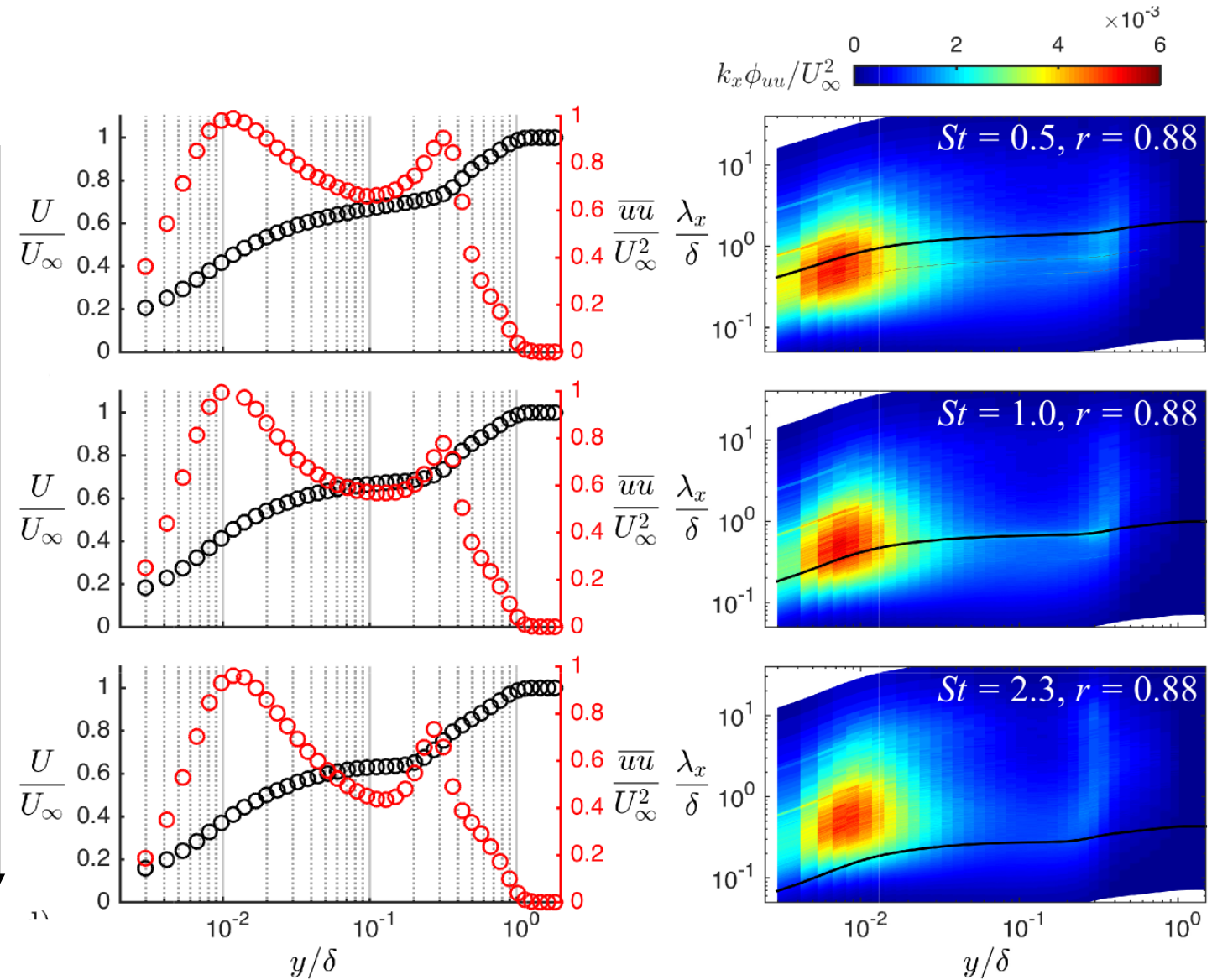


Constant  $St$   
Varying  $r$

# Turbulent Spectra

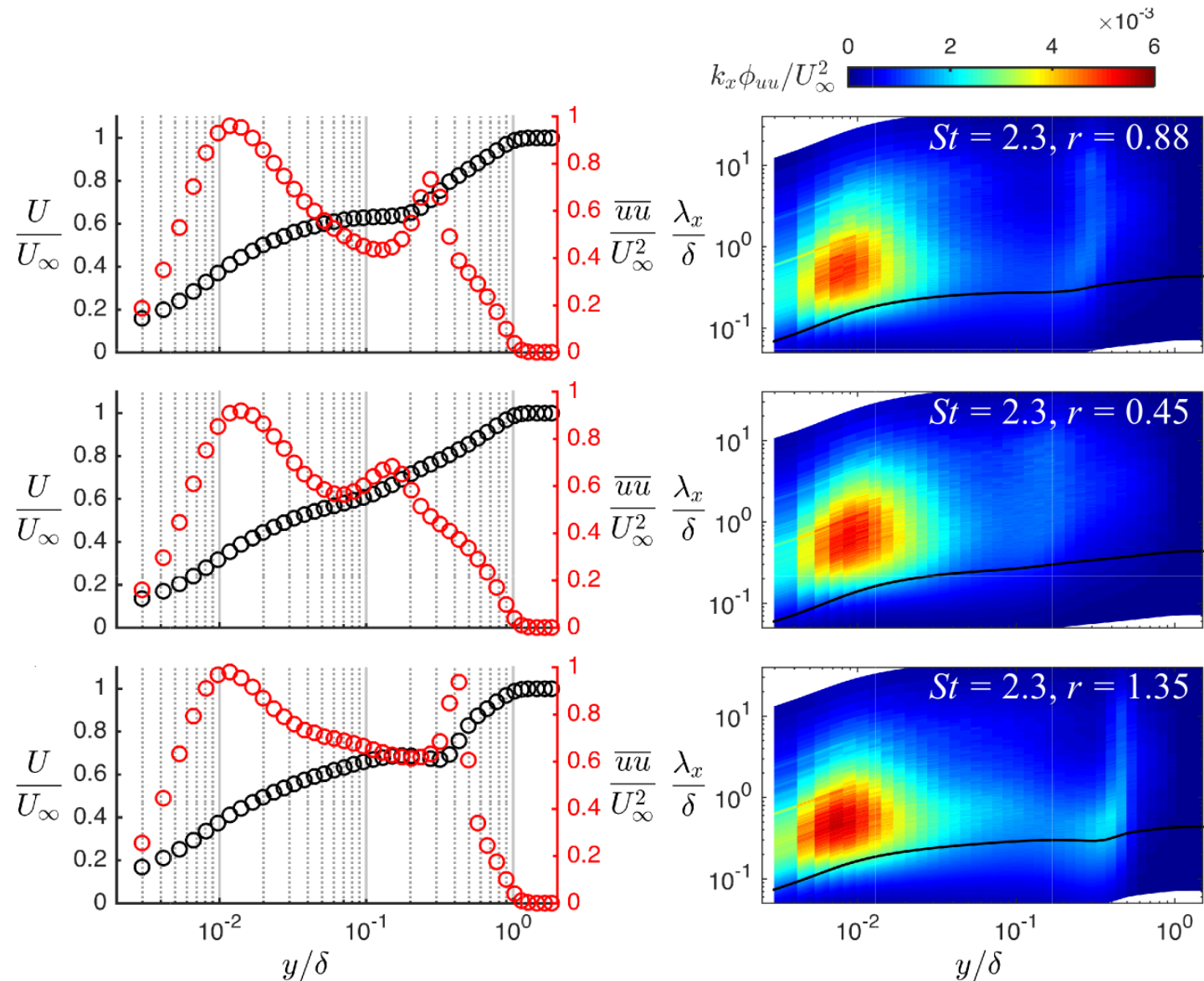
- Larger effect on log region with lower Strouhal numbers

Constant  $r$   
Increasing  $St$



# Turbulent Spectra

- Increased blowing ratio increases the  $y$  of max input of streamwise turbulence intensity
    - Increased jet penetration
- Constant  $St$   
Varying  $r$
- Larger effect on log region with larger blowing ratios

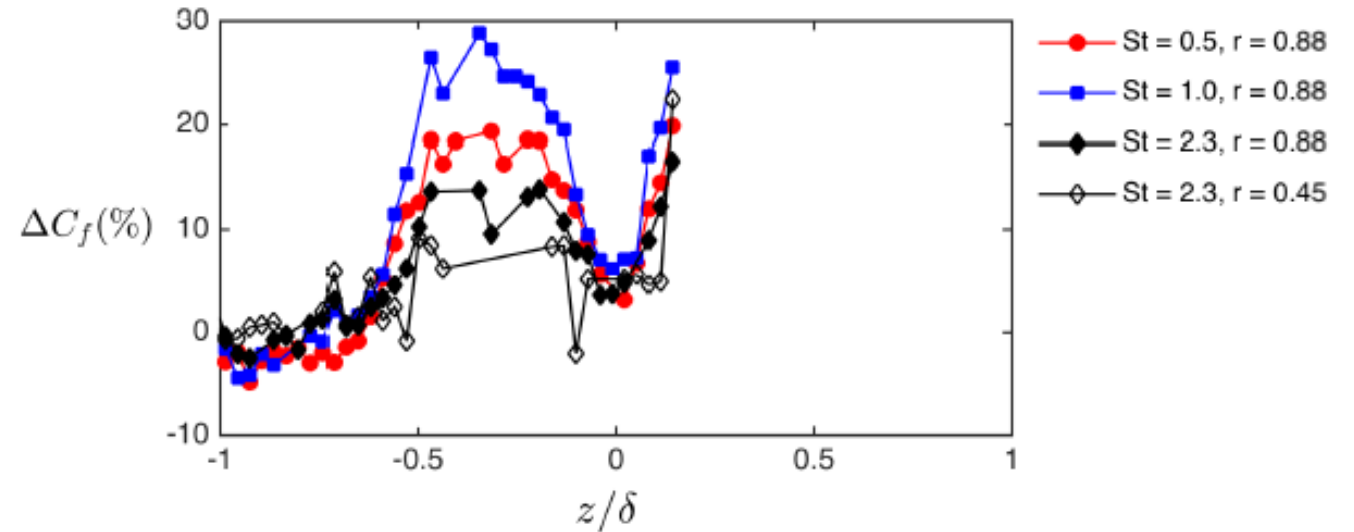


# Skin Friction Measurements

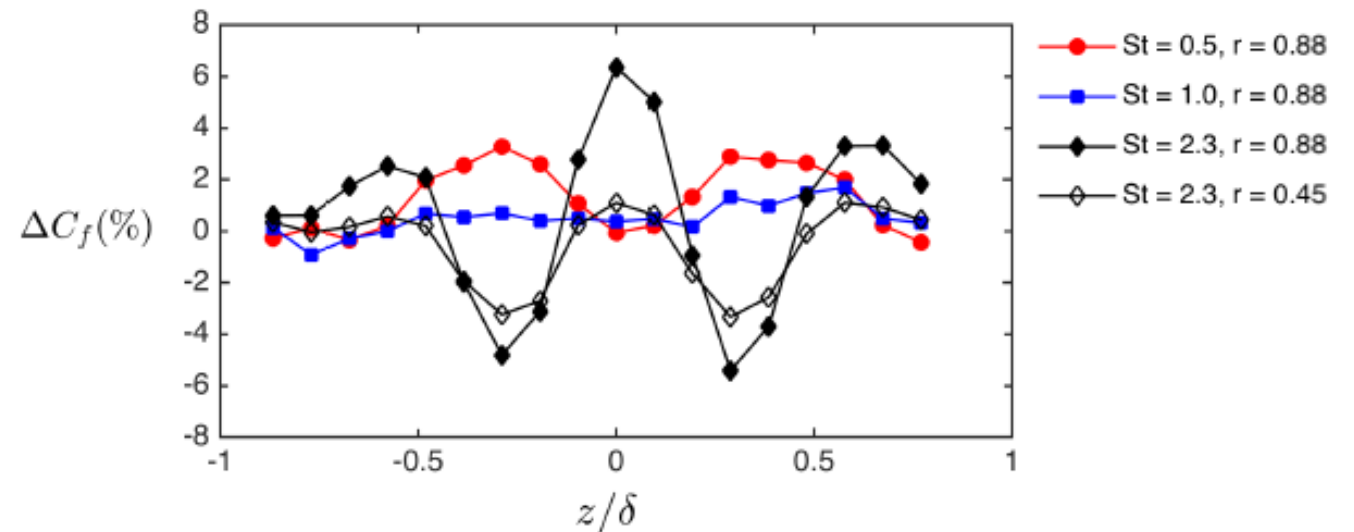
- Net skin friction reduction at  $x/\delta = 5$  downstream of jets for  $St = 2.3$ ,  $r = 0.45$
- Lower blowing ratio preferred
- Clauser chart fit:

$$\frac{U}{U_\tau} = \frac{1}{\kappa} \log \left( \frac{y U_\tau}{\nu} \right) + A$$

Constants:  $\kappa = 0.41$ ,  $A = 5.0$



(a)  $x/\delta = 1.5$  oil film interferometry data.

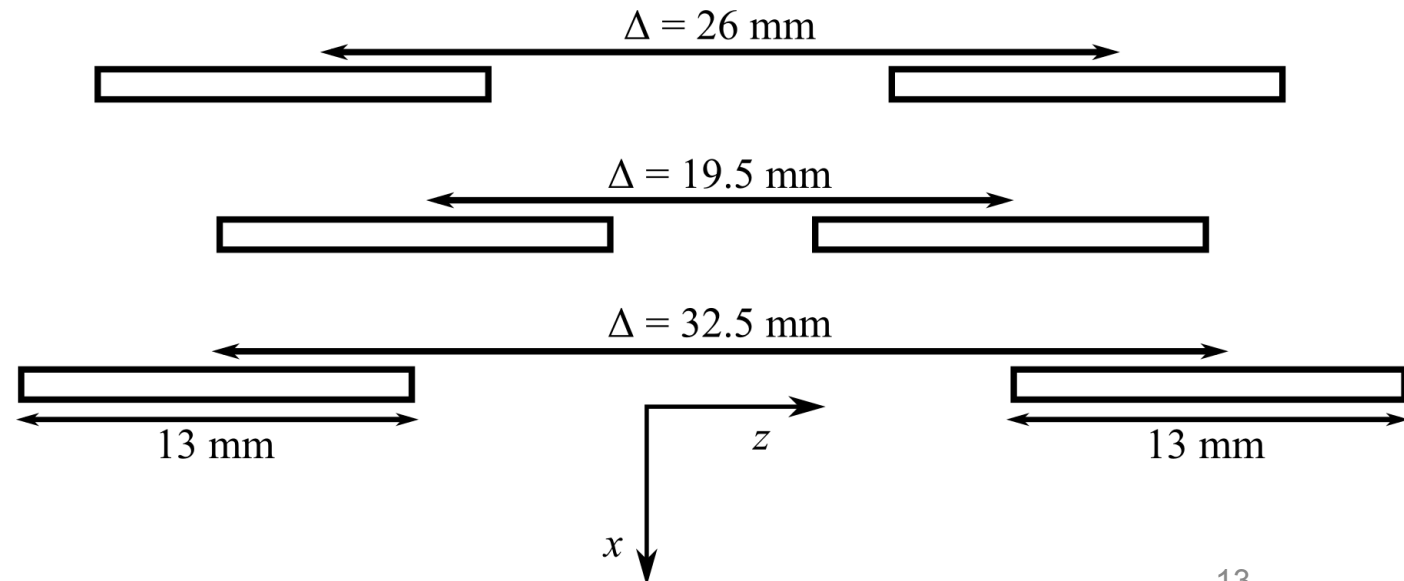


(b)  $x/\delta = 5$  Clauser chart measurements of the skin friction.

# Skin Friction Parameter Mapping

- 3 parameters investigated:
  - Strouhal number,  $St$
  - blowing ratio,  $r$
  - jet spacing,  $\Delta$
- Additional measurements at low  $St$  and  $r$  as necessary
- $C_f$  measured at 6 locations behind jets

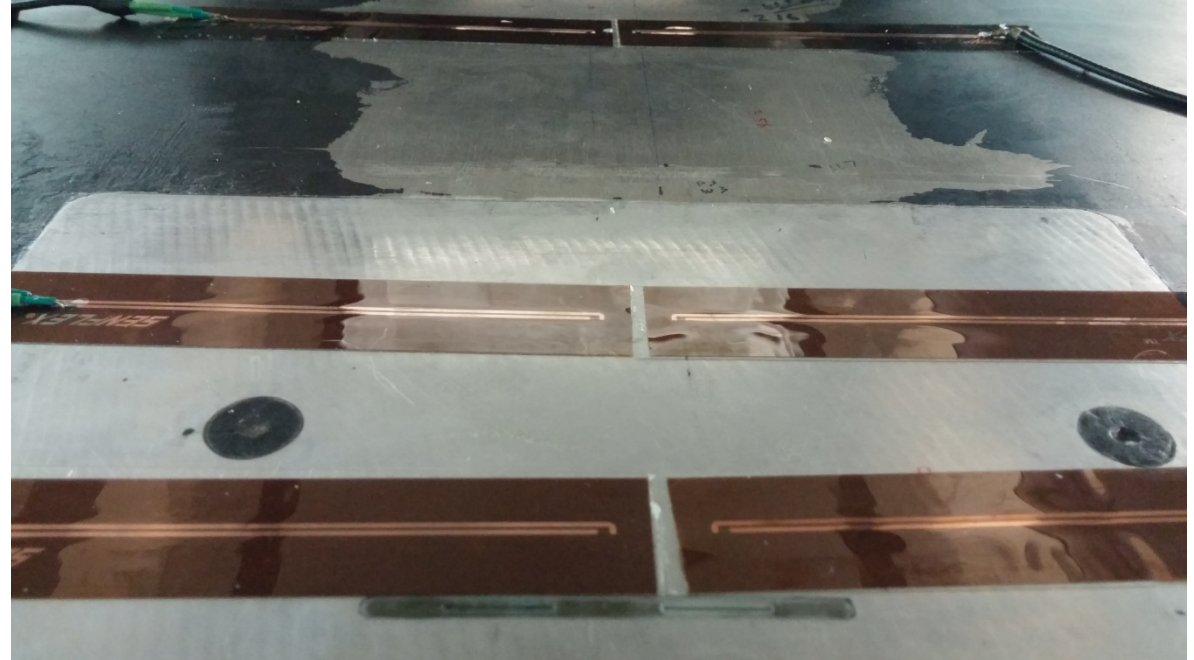
Parameter	Min	Max	# Points
$St$	0.042	2.7	14
$r$	0.1	1.4	14
$\Delta/\delta$	0.46	0.76	3





# Hot Films

- Nickel sensing element
- Copper leads
- Polyimide substrate
- 120 x 20 x 0.127 mm
- 6 total: 3 streamwise locations ( $0.33\delta$ ,  $1.5\delta$ ,  $5\delta$ ) x 2 spanwise locations (behind jet, between jets)
- Controlled with a CTA at overheat ratio of 1.4 – 1.6
- Calibrated before and after measurements to account for drift



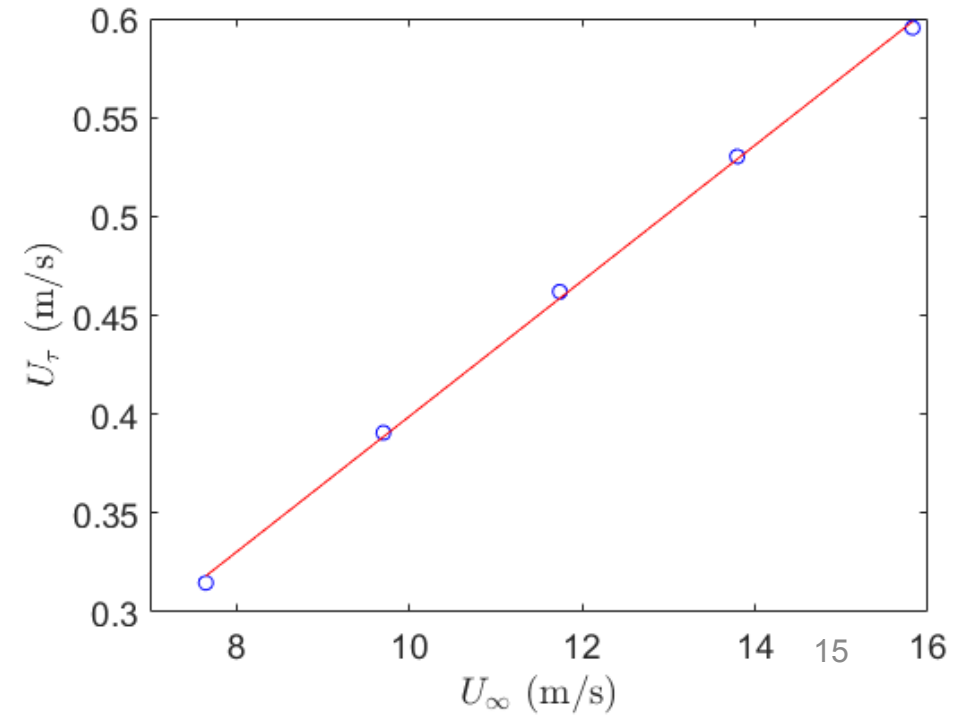
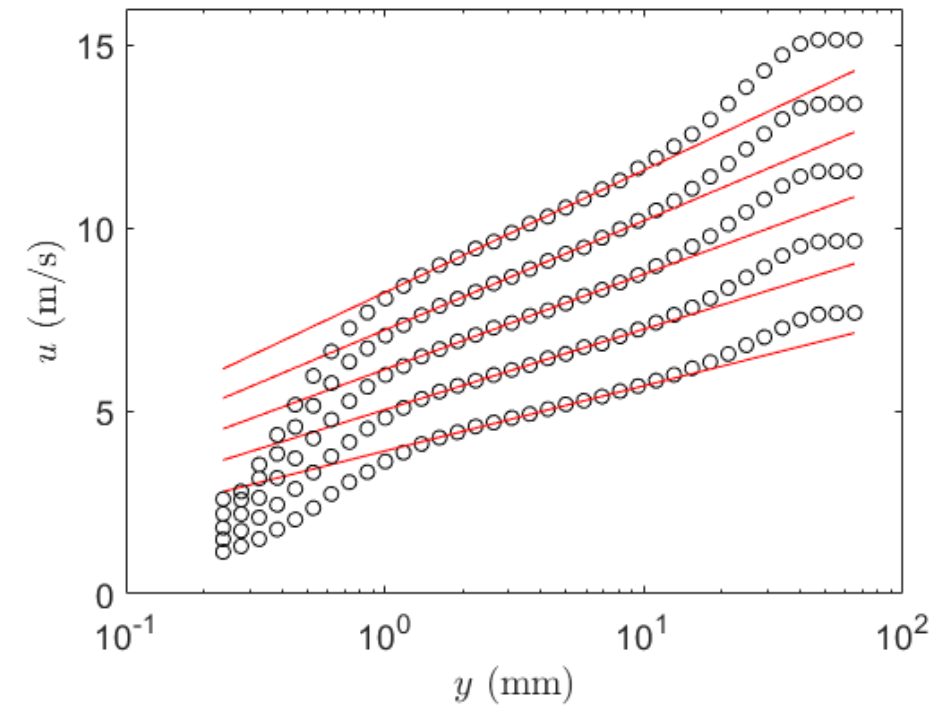
# Shear Stress Calibration

- Measure BL profiles at range of
- Extract  $U_\tau$  using a Clauser chart fit to log region of each profile:

$$\frac{U}{U_\tau} = \frac{1}{\kappa} \log \left( \frac{y U_\tau}{\nu} \right) + A$$

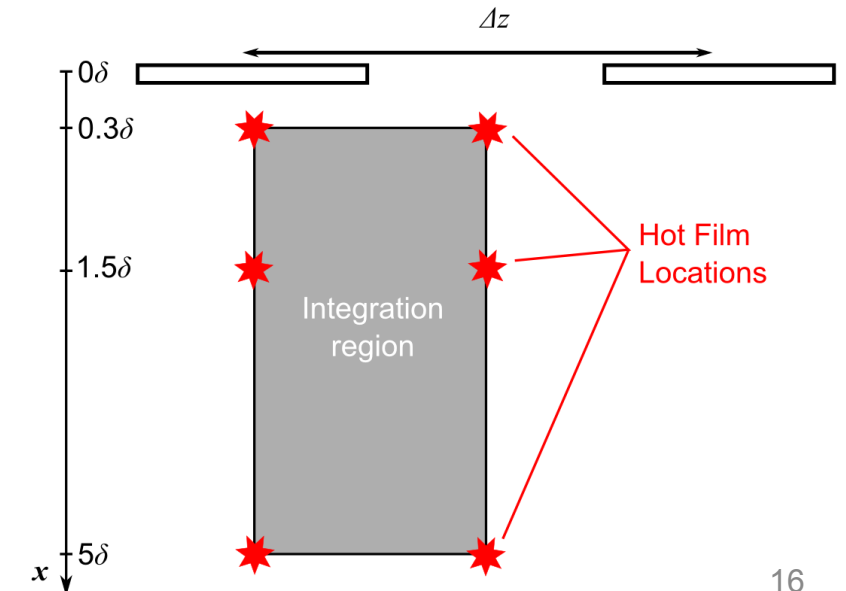
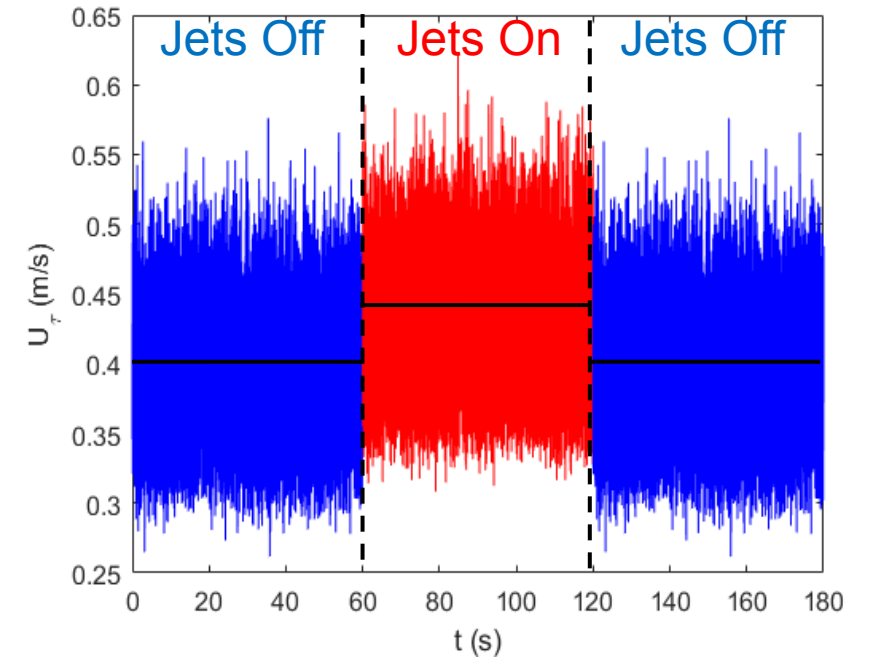
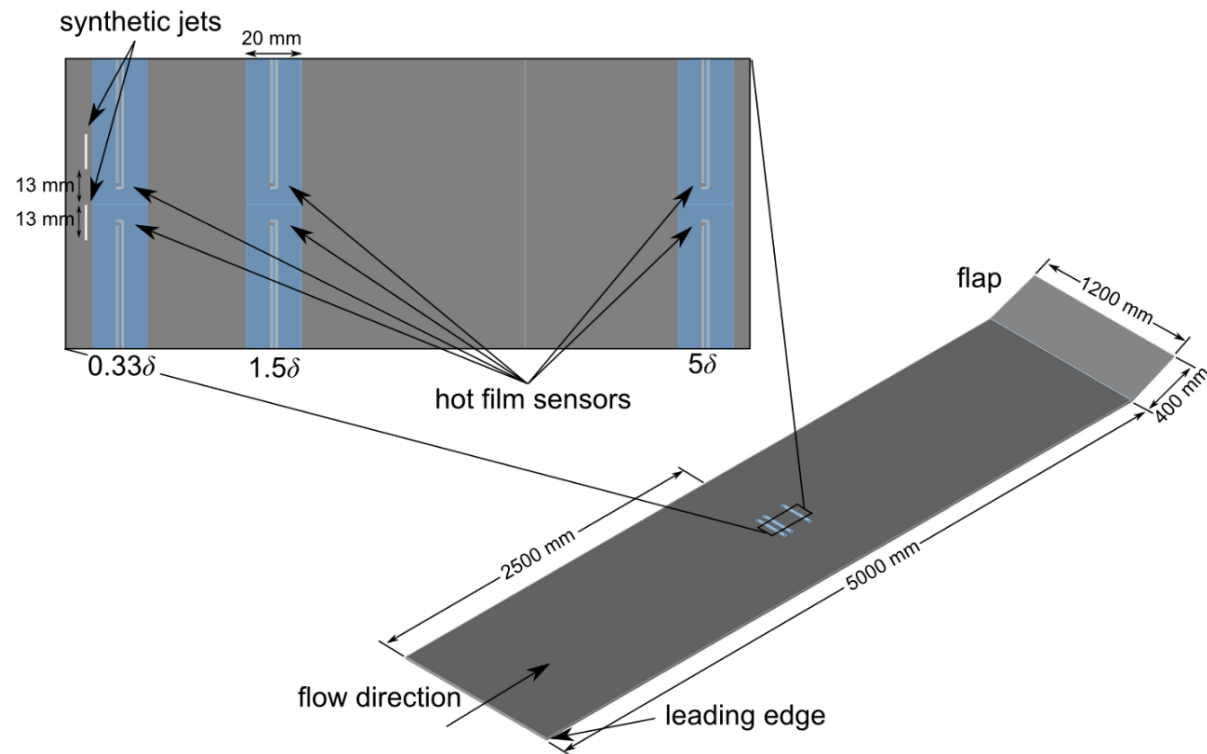
Constants:  $\kappa = 0.41$ ,  $A = 5.0$

- Extract parameters of fit to  $U_\tau$  vs.  $U_\infty$
- Independently done at location of each hot film

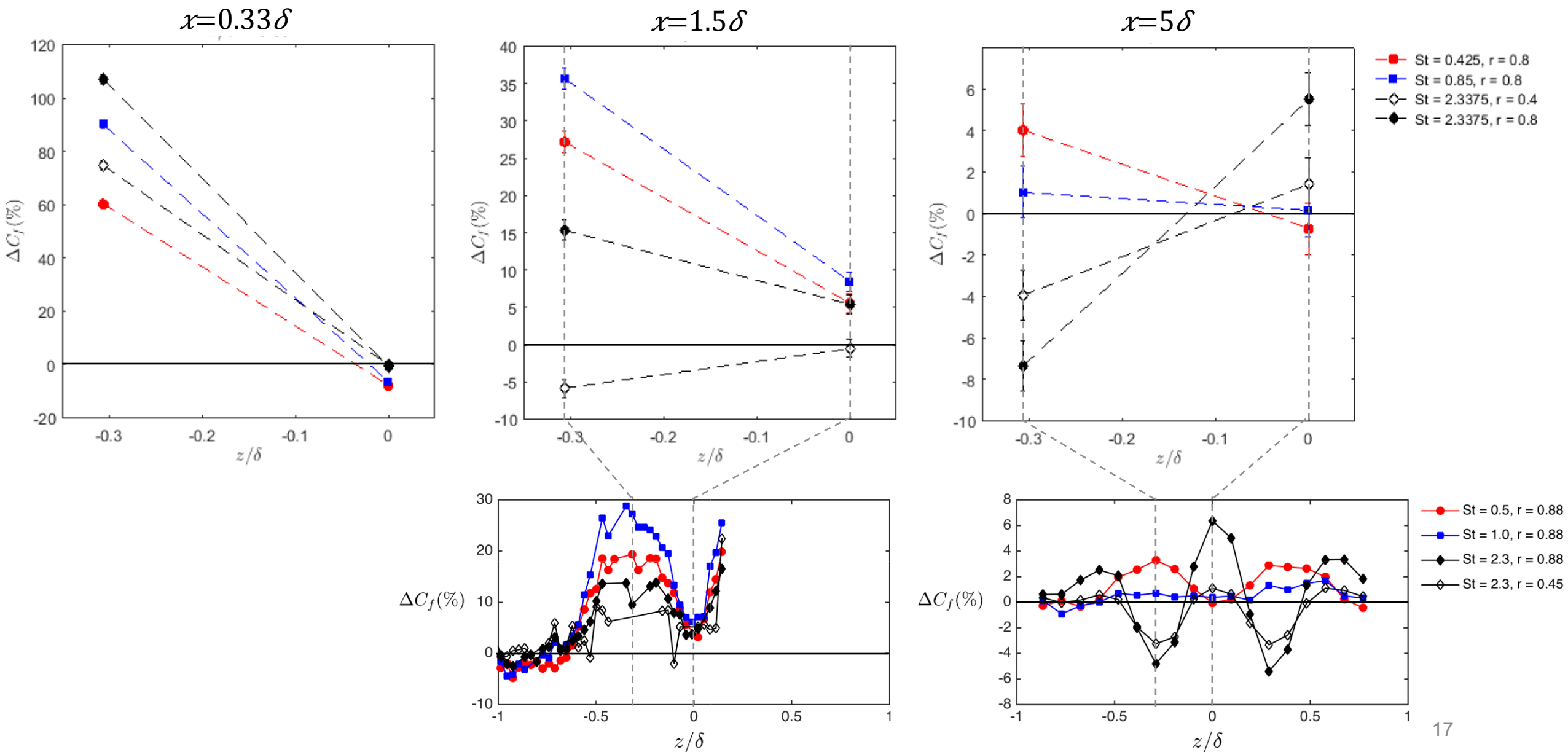


# Skin Friction Measurements

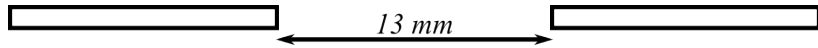
- Measure mean shear stress before, during, and after actuation at the 6 measurement locations
- Calculate  $\Delta c_f = \frac{\tau_w - \tau_{w0}}{\tau_{w0}} \times 100\%$
- Integrate over the 6 points with a simple trapezoidal integration



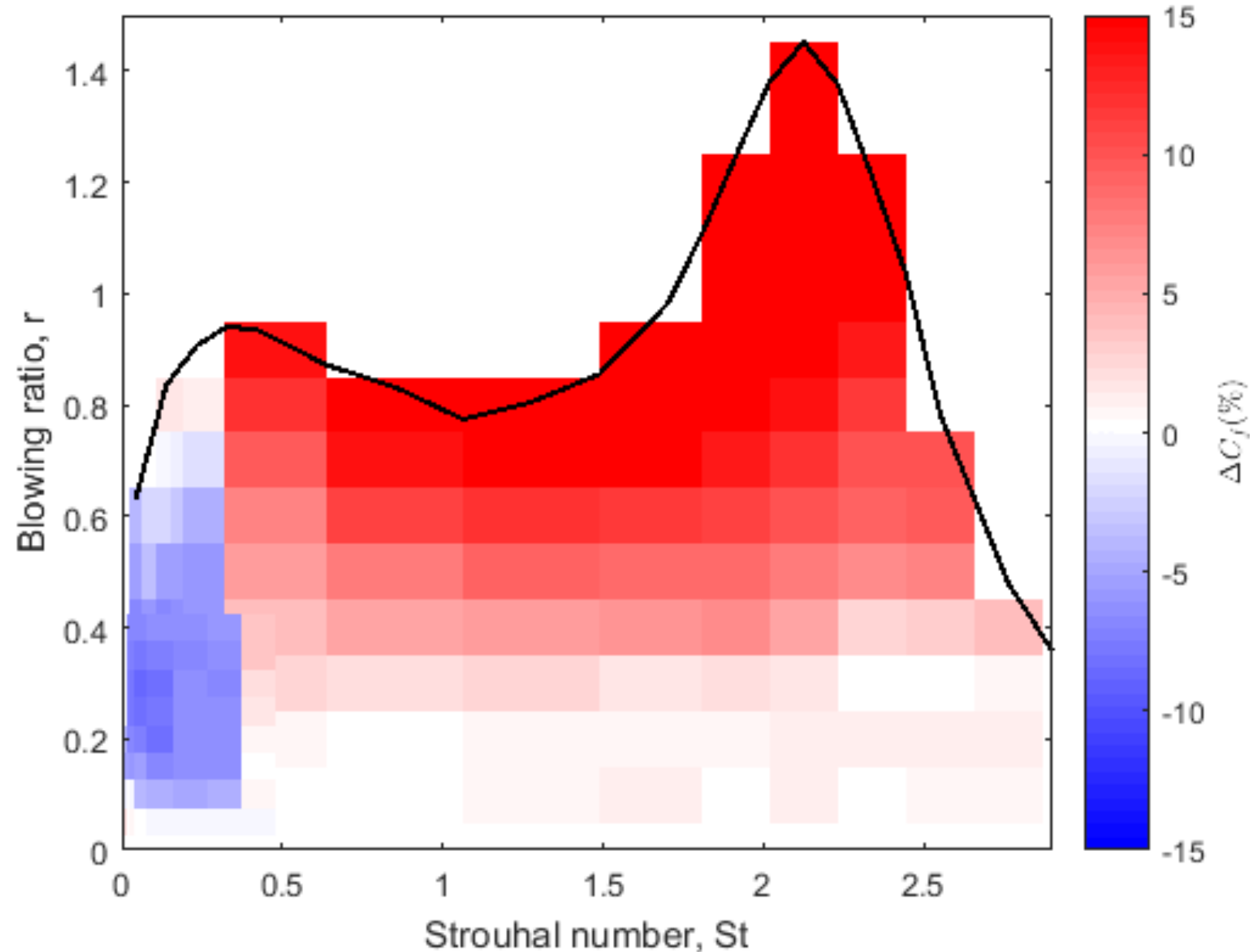
# Comparison with OFI and Clauser chart



# 13 mm spacing – Parameter map

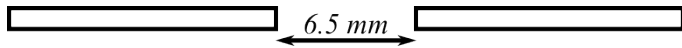


- Region of reduced skin friction centred at  $(St, r) = (0.043, 0.25)$
- High blowing ratio results in skin friction increase
- Skin friction increase also at Strouhal number above 0.5

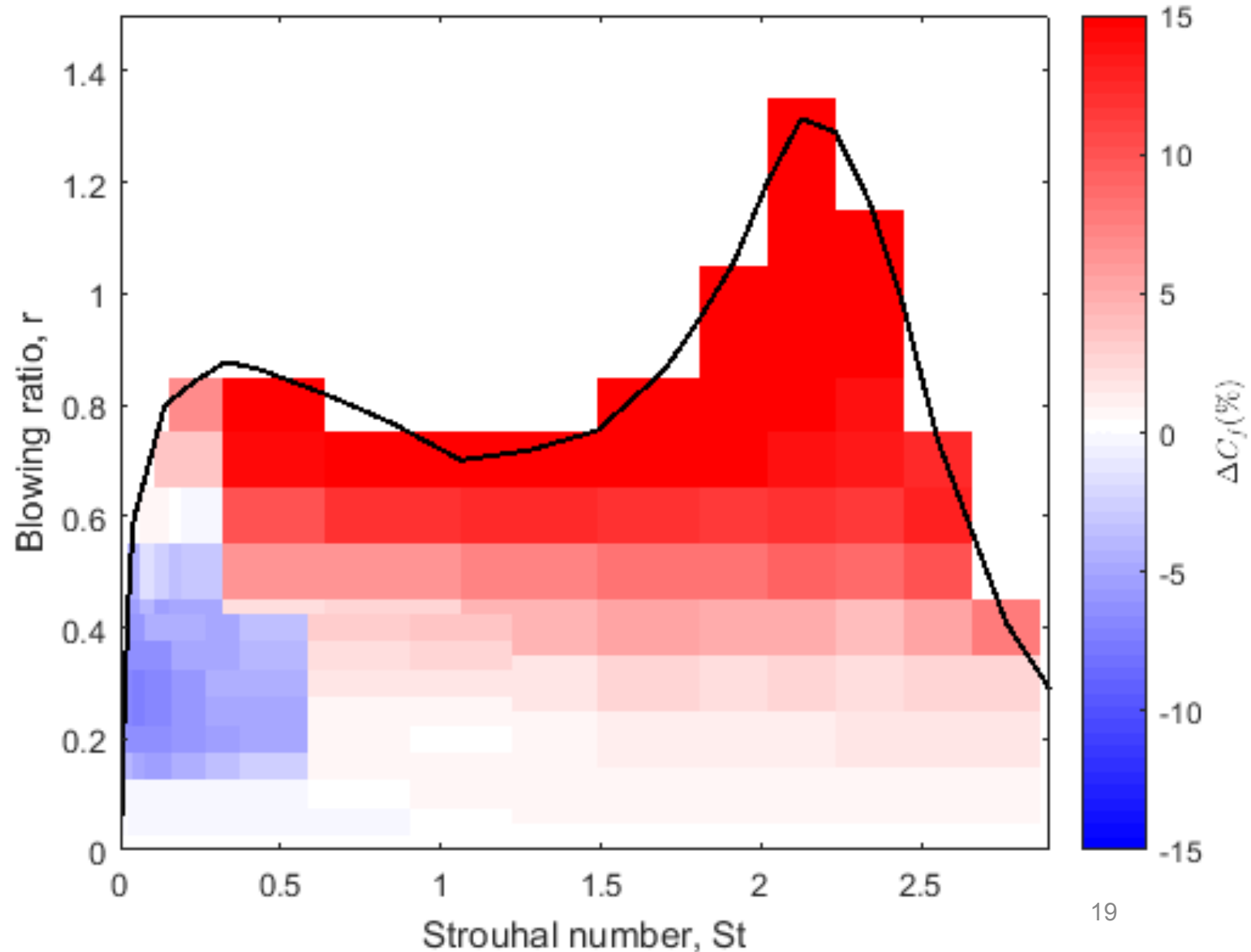




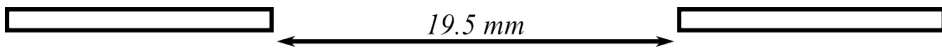
# 6.5 mm spacing – Parameter map



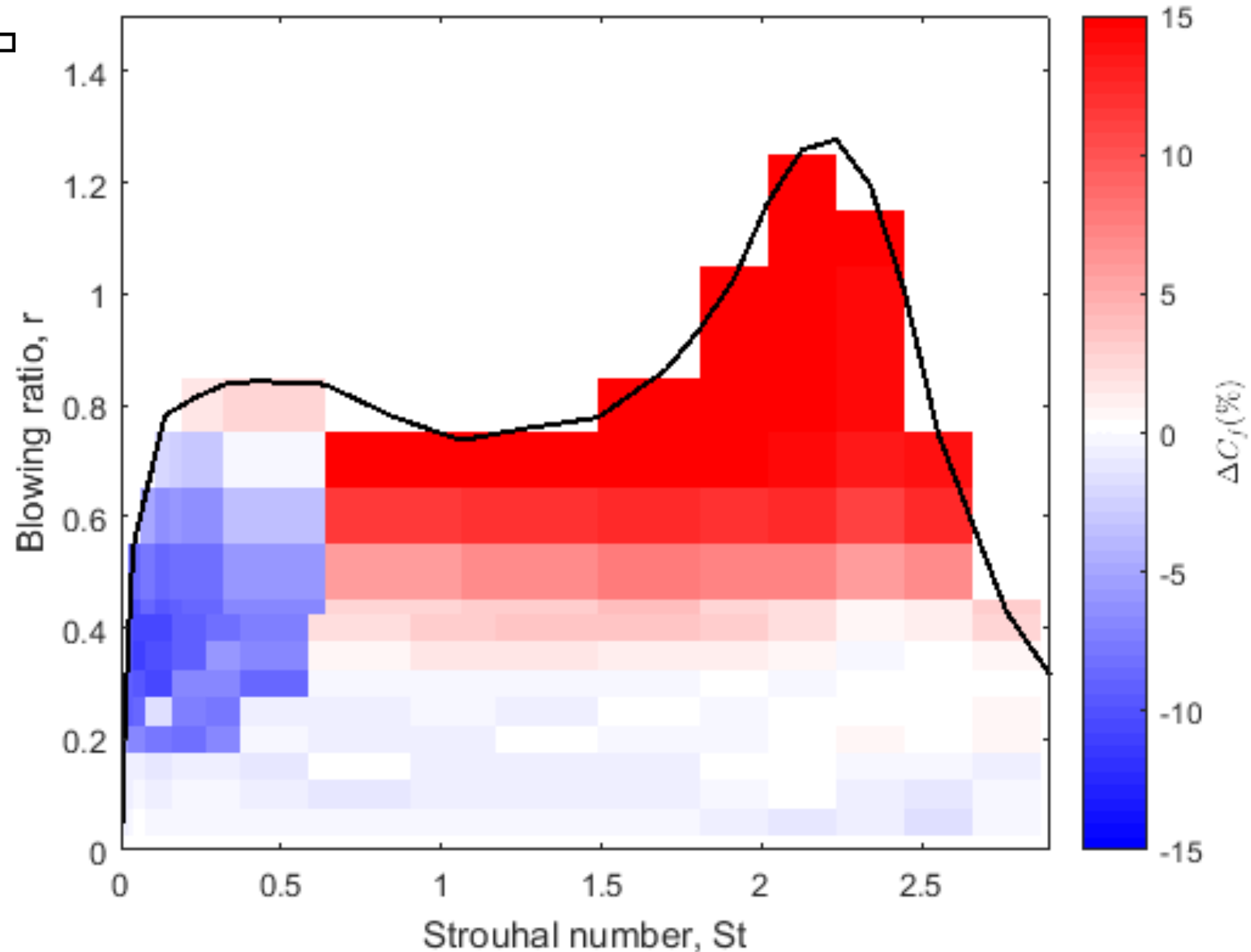
- Region of expected reduced skin friction centred at  $(St, r) = (0.032, 0.3)$
- Nearly identical to the results with the 13mm spacing
- Slightly larger region of reduced skin friction



# 19.5 mm spacing – Parameter map

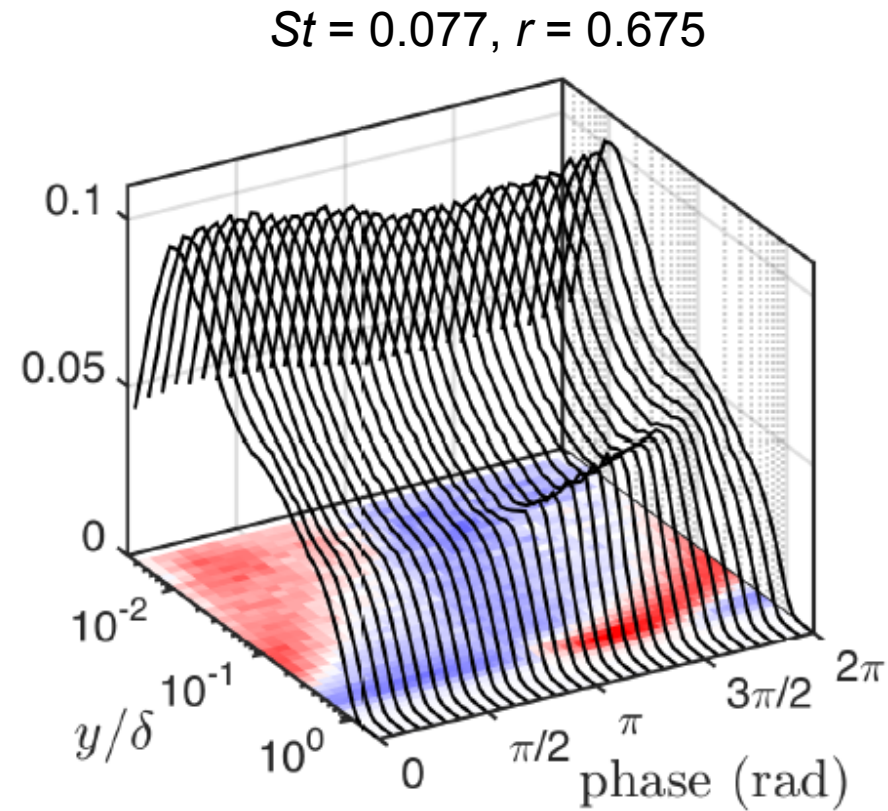
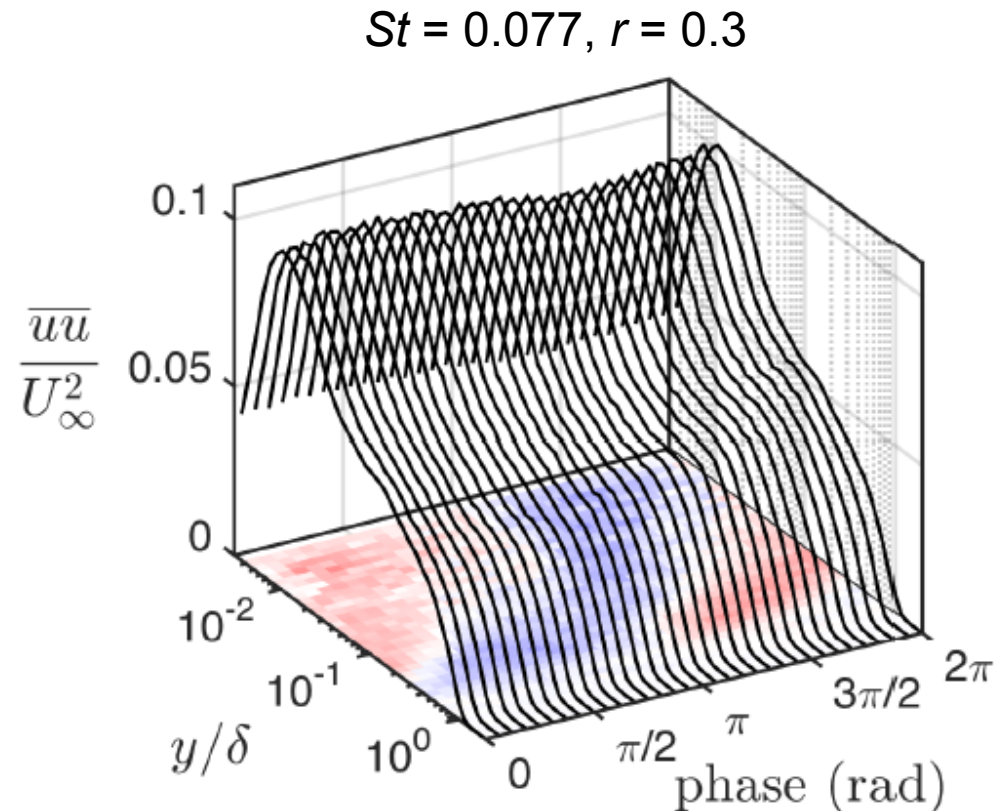


- Region of expected reduced skin friction centred at  $(St, r) = (0.0425, 0.35)$
- Similar to the results with the 13mm and 6.5mm spacing
- Region of expected skin friction reduction is larger
  - Seemingly Strouhal number independent at low blowing ratio



# Low Frequency Forcing

- Amplitude modulation of near wall peak due to structures imparted by the synthetic jets
- Effect increases with increasing blowing ratio



# Conclusions

- Skin friction increases with increasing Strouhal number and blowing ratio
- Largest “decrease” in skin friction centred around  $St = 0.04$  and  $r = 0.3$
- Amplitude modulation of synthetic jet structures on near wall peak
- Low Strouhal number and high blowing ratio causes largest input of streamwise turbulence intensity
- **Low frequency forcing most effective at manipulating boundary layer**

# Questions?