



Assessment of steady-state losses in electrical drives

Giampaolo Torrisi, Dr. Sebastien Mariethoz, Prof. Roy Smith
Automatic Control Laboratory – ETH Zurich

Introduction

Field Oriented Control

Dynamic performance

Constant nominal flux

Non-optimal for losses

Model with linear inductances

Sufficient for basic control

A non-linear model for the inductances is necessary to optimize losses

Induction Motor modeling

Model with linear inductances

$$\dot{x}^f = A_c x^f + B_c u^f + A_{sc} \omega_s x^f + A_{rc} \omega_r x^f$$

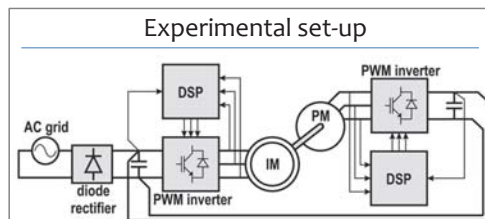
$$x^f = [\psi_{ra} \ \psi_{r\beta} \ i_{sd} \ i_{sq}]'$$

$$u^f = [u_{sa} \ u_{s\beta}]'$$

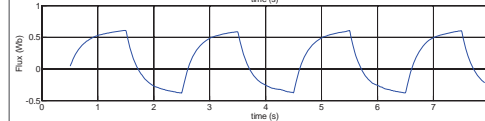
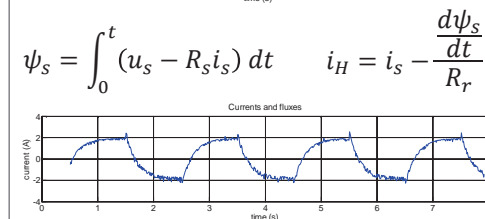
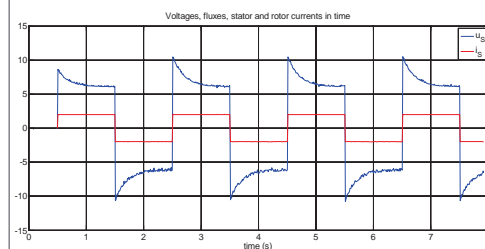
Needs an accurate model

- Unavailable from manufacturer
- Theoretical Jiles-Atherton relations
- Experimental evaluation

Experimental test for saturation



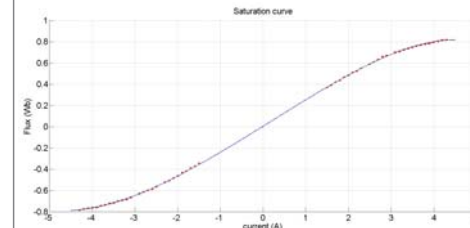
i_{sd}	Alternating I_{ref} or $-I_{ref}$
i_{sq}	0 (no torque)



$$\psi_s = \int_0^t (u_s - R_s i_s) dt \quad i_H = i_s - \frac{d\psi_s}{R_r}$$

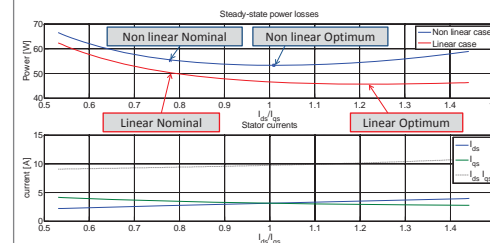
Steady-state optimal currents

Inductances with saturation effect



We assume L_r and L_m to be proportional to L_s

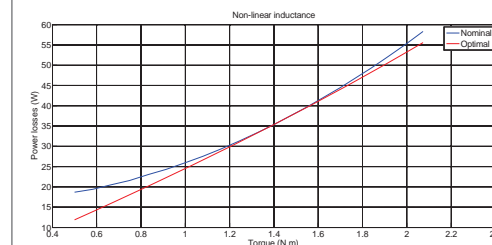
Optimization of stator currents



- up to 21% losses mismatch with linearity
- 4% improvement assuming non-linearity
- 3.5% more losses if linear optimum was implemented instead of non-linear one

Improvements in efficiency

Losses as a function of the torque



Improvement in drive efficiency:

- Rated power: 0.3 – 1.2%
- Low power, 4 - 16%

Future work

- Real-time control of stator currents to achieve dynamically theoretical savings
- Capability to optimally control varying loads known in advance
- Take in account hysteresis and iron losses

